

# **STRATFORD FAIRGROUNDS**

# **Conceptual Servicing Report**

Project Location: Stratford, ON

Prepared for:



December 5, 2014

Rev. January 20, 2015

Issued. February 20, 2015

MTE File: 37888-300



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## 1.0 INTRODUCTION AND BACKGROUND

MTE Consultants Inc. has been retained by the City of Stratford to prepare a preliminary servicing report to address the servicing requirements to transfer the land use for the property located at Part of Lot 3, Concession 1 from a recreational 'fairground' use to a residential use complex, refer to Figure 1 for site location.

This report is prepared to demonstrate that the overall proposed development is serviceable with the existing and proposed infrastructure and roads adjacent to the development. This report identifies the servicing required to facilitate the proposed development.

In addition to providing a servicing strategy for the overall parcel of land, the report provides the framework and design parameters for the development of future community facilities (namely a storm water management block and sewage pump station).

Refer to Figure 2 for the conceptual land use plan of the development provided by the City of Stratford with minor modifications made to reflect the proposed design for the site.

## 2.0 EXISTING CONDITIONS

The subject lands comprise of approximately 11.50 hectares of vacant lands that are bounded by the Rotary Recreational Complex to the north, Britannia Street to the south, and residential subdivisions to the east and west. The site previously was the home of the Stratford fairgrounds. All buildings have been removed and a record of site condition is available for this Brownfield site.

The subject property is generally gently sloping in a northerly direction. The existing topographic mapping identifies a total elevation difference of approximately 2m over the entire length of property or an average slope of less than 1%. In accordance with the geotechnical information in this area, the soils consist of generally silt, sand and glacial till. A limited amount of topsoil is available on the site due to its past land use and the remediation works completed. Groundwater depth should be confirmed.



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## 3.0 PRELIMINARY SITE GRADING

A preliminary grading design has been completed for the proposed development concept plan as follows:

- Preliminary grading complete to maintain the existing overland flow routes entering the site and drainage to SWM facility; and
- Preliminary grading design for the SMM Facility; and
- Preliminary cut/fill calculation for overall site.

Refer to Figure 3 for the conceptual cut/fill analysis based on the preliminary grading design. It should be noted that there is a surplus of fill generated from the 'Fairground' site works of approximately 47,000 cubic meters. This excess fill can be used to reinstate the dry SWM pond facility beside the Rotary Recreational facility and to level the existing ball fields.



		Dec 04 2014 13.6	9PM; Grid size: 2.5;	Base Surface: OG;	Finish Surface:FG		
Area#	tot_Area	topsoil	cut	fill	net	stripping	pregrade
ID	m2	m3	m3	m3	m3	depth	depth
MTE_PARCEL : 1	8056.250	0.000	1293.780	2134.817	-841.0	0.0	0.7
MTE_PARCEL : 2	3906.250	0.000	743.071	1316.986	-573.9	0.0	0.7
MTE_PARCEL : 3	9868.750	0.000	4616.206	322.891	4293.3	0.0	0.7
MTE_PARCEL : 4	16331.250	0.000	2267.895	6147.298	-3879.4	0.0	0.9
MTE_PARCEL : 5	6175.000	0.000	1337.663	106.765	1230.9	0.0	0.9
MTE_PARCEL : 6	8412.500	0.000	2100.799	140.665	1960.1	0.0	0.9
MTE_PARCEL : 7	3606.250	0.000	716.433	524.453	192.0	0.0	0.9
MTE_PARCEL : 8	3618.750	0.000	1763.959	181.489	1582.5	0.0	0.9
MTE_PARCEL : 9	17712.500	0.000	12597.409	4.668	12592.7	0.0	0.9
MTE_PARCEL : 10	11712.500	0.000	30546.186	0.973	30545.2	0.0	0.3
totals:	89400	0.0	57983.4	10881.0	47102.4		





PARCEL NUMBER

CUT CONTOURS FILL CONTOURS ZERO ELEVATION CONTOURS



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# 4.0 SANITARY SERVICING

## 4.1 Existing Sanitary Servicing

The existing fairground site was serviced to Britannia Street by two sanitary services and to Glastonbury Drive by one 150mm service. Both services have been disconnected with the completion of the demolition of the site. These existing sanitary services are not suitable for the proposed subdivision development due to limited depth and size. There is an existing 200 sanitary main in front of the site on Britannia Street which conveys flows easterly to the Churchill Circle and John Street.

## 4.2 Proposed Sanitary Servicing Strategy

Various options have been examined to determine the most feasible and cost effective means to service the proposed plan of subdivision. Options for gravity sanitary drainage of the site are limited. Existing sewers on the adjacent streets (Briarhill, Glastonbury, Britannia, Coriano and Waddell) are at capacity, too shallow for connections or are not accessible from this site. An existing 375mm diameter sewer exists on Britannia Street near Briarhill Drive.

In order to connect the entire development site to this sewer, the site would be required to be graded from north to south. This would require significant fill at the north end of the site. Additionally due to very limited overland flow capacity within the major storm drainage sub-catchments, the City of Stratford will not permit significant changes to these sewer catchment areas.

In addition to reviewing a number of gravity servicing options, MTE has also reviewed several sanitary pumping options and configurations to service the development. The recommended sanitary solution includes the construction of a small pump station adjacent to the proposed SWM facility and Street 'B'. This pump station is located centrally on the site and located to permit local sewers at a minimal depth to drain to it.

Refer to Figure 4 for the existing and proposed sanitary servicing strategy.



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## 4.3 Proposed Sanitary Pump Station

The Fairgrounds Sanitary Pumping Station (FSPS) is designed to service new residential development lands at the former fairgrounds site in the City of Stratford. The preliminary sizing is specific to the concept that was provided by the City of Stratford, alternative concepts may result in different sizing requirements.

The pump station is being proposed to be located on the future Street 'B' adjacent to the proposed SWM facility for the development. A single sanitary forcemain will extend southerly from the pump station along the future Street 'B' and will outlet to an existing gravity sewer.

Two potential gravity outlets for the discharge of the sanitary forcemain were examined. The first location is the manhole located on Glastonbury immediately north of the Churchill roundabout. From this manhole sanitary flows are conveyed via an existing 375mm sanitary sewer to John Street. It has been determined that the downstream sanitary sewer at this location does not have sufficient capacity to accommodate the proposed subdivision.

The second discharge location examined was the existing manhole at the intersection of John Street and Charles Street. From this manhole wastewater is conveyed downstream southerly on John Street via an existing 450mm sanitary sewer. MTE has confirmed that this discharge location is preferred and has suitable capacity for the conveyance of the flows from the proposed pump station. Refer to Figure 5 for a concept plan of the preferred forcemain routing on John Street.

From this preferred location, wastewater will be conveyed by the gravity sewer system which ultimately outlets to the Stratford Wastewater Treatment Plant.

# 4.4 DESIGN PARAMETERS

## 4.4.1 Design Guidelines

The following is a summary of the design parameters for the Fairgrounds SPS:

**Design Flow rates** as per The Engineering Design Criteria Manual for the City of Stratford and the *MOE Design Guidelines for Sewage Works (2008)* an average daily per capita flow of 345.6 L/person/day with an infiltration allowance of 0.10L/s/ha is to be used for sewage calculations. Based upon the preferred development concept plan, the total population for the development is 145 units. As per the City of Stratford design guidelines, the population density is 2.4 pp/unit. Therefore the total design population for the proposed development in 348 persons. The Harmon Peaking Factor has been applied to calculate the peak design flow rate for the entire catchment area.

**Pumping Station and Forcemain Design Standards** as per the *MOE Design Guidelines for Sewage Works (2008),* and;

**Standby Generator Set** as per the Ministry of Environment Standard Specification for Diesel Engine Generator Sets (MOE Spec No. 2, June 1981). The standby generator specified for the Fairgrounds SPS will be required to be registered through the Environmental Activity and Sector Registry (EASR).

## 4.4.2 Design Flow Rate

The design flow rates for the Fairgrounds SPS have been determined based upon the preferred conceptual land use plan.

The Harmon Peaking Factor has been applied to calculate the peak flow rate of 6.41 L/s. Refer to Appendix A for the drainage area plan and the design flow rate calculation.

The design flow rates for the Fairgrounds SPS are summarized as follows:

Peak Flow	6.41 L/s
Average Flow	2.17 L/s

## 4.4.3 Wet Well Sizing

In accordance with the *MOE Design Guidelines for Sewage Works (2008)*, the new wet well has been sized based on a minimum 10 minute cycle time. The required wet well volume was determined based on a single pump system plus one redundant backup pump of equal size. Wet well sizing is discussed further in Section 4.5.4.

## 4.4.4 Firm Capacity and Forcemain Velocities

A total of two pumps, one duty and one standby, are proposed to be provided in the Fairgrounds SPS. In accordance with the *MOE Design Guidelines for Sewage Works (2008)*, the firm pumping capacity has been established based on the standby pump being out of operation. The station's design capacity is 7.5 L/s; which is slightly larger than the required design flow. The proposed 100 mm diameter forcemain will maintain velocities within the MOE recommended range of 0.6 m/s to 3.0 m/s. It should be noted that a minimum velocity of 1.1 m/s is generally preferred to ensure solids remain in suspension, and once the velocity exceeds 2.6 m/s, measures should be taken to provide additional forcemain capacity within the system. Pump and forcemain sizing is discussed further in Section 4.5.3.

## 4.5 PUMPING STATION DESIGN SUMMARY

# 4.5.2 Description

The Fairgrounds SPS is to be located on a block in the former fairground site, Stratford, ON. The Site is approximately 700 m north of the Churchill Roundabout. The block size will be required to approximately  $20m \times 20m$  and the building size should be approximately  $6 \times 8 m$ . The Site will be serviced with water and three phase electrical power. The preliminary construction cost for the SPS and forcemain is approximately \$1.05 million.

The pumping station construction should consist of a pre-cast 1.8 m diameter wet well, separate metering chamber, control building, standby diesel generator set, submersible sewage pumps, magnetic flow meter, forcemain bypass, process piping air release valve and PLC based control system connected to the City SCADA system.

# 4.5.3 Pumps Capacity and Forcemain

ITT Flygt submersible pumps have been sized to accommodate the peak design sewage flow rate of 6.41L/s. Two identical pumps will be used (one duty and one stand by), each with an independent capacity of 7.5 L/s to provide the station's firm capacity 7.5 L/s. During normal operation, the sewage level will oscillate between predetermined level set points. The pumps should have rotational duty such that there is equal use of each pump.

The two pumps are arranged to discharge through two 75 mm diameter pipes. These pipes will enter a separate metering chamber located approximately 1.0 meter downstream of the wet well. A combination air/vacuum release valve is provided in the metering chamber for each pump discharge line.

Within the metering chamber, the two pump discharge pipes will join into a common 100 mm diameter header which passes through a magnetic flow meter. Once leaving the metering chamber, the single 100 mm diameter outlet piping will connect into the 100 mm diameter forcemain.

A single 100 mm diameter discharge forcemain is recommended to be installed from the valve chamber to the existing gravity discharge outlet manhole located at John Street and Charles Street.

The downstream sewer at this location has sufficient capacity to accommodate the additional peak flow (6.42 l/s) from the proposed development and the construction cost and complexity to install the forcemain at this location should be reasonable if it can be kept in the boulevard.

# 4.5.4 Wet Well Sizing

The proposed wet well will be a single 1.8 m diameter precast concrete manhole. *MOE Design Guidelines for Sewage Works (2008)* recommend that the sewage wet wells be sized to allow a minimum 10 minute cycles times, which is equivalent to six pump starts per hour. It is also recommended that the time required to fill the wet well volume not exceed 30 minutes based on the average design flow rate of 2.17 L/s

In order to accommodate the pumping capacity of 6.41 L/s, the required working wet well volume was calculated using the following equation:



A cycle time of 10 minutes was utilized, with the single duty pump able to accommodate a pumping capacity of  $0.45 \text{ m}^3/\text{min}$ . This corresponds to a wet well volume of  $3.68 \text{ m}^3$ . The total area of the 1.8 m diameter wet well is  $4.5 \text{ m}^2$ . In order to provide a working wet well volume of  $3.68 \text{ m}^3$  with a wet well area of  $4.5 \text{ m}^2$  the wet well needs to have a minimum operating depth of 0.81 m. Since this is a single duty pump system (with one standby pump) the required operating depth is measured from the duty pump ON sewage level to the pump OFF sewage level within the wet well.

To allow for storage volume within the wet well and the potential for increasing the service area of the Fairgrounds pumping station in the future, the station design allows for an operating depth of approximately 1.0 m, which provides sufficient operating volume in the wet well to ensure the pumps operate with a minimum cycle time of greater than 10 minutes. An operating depth of 1.0 m provides a working wet well volume of  $4.5 \text{ m}^3$ , which corresponds to a fill time of approximately 10.2 minutes based on an average design flow rate of 2.17 L/s.

The precast wet well is to be approximately 6.0 m deep from finished grade to underside of structure. The wet well sizing calculations are contained in Appendix A.

## 4.5.5 Ventilation

A continuous power heated ventilator will be installed on the wet well lid to provide positive air displacement to the wet well at all times. A single gooseneck vent will allow for the air to dissipate to the atmosphere and minimize the accumulation of odour causing gases in the wet well. The heater ventilator will prolong the service life of the wet well by reducing corrosion of metals and concrete. The heat is necessary to prevent freezing during the winter while still allowing pressurized ventilation.

## 4.5.6 Emergency Generator

A diesel 40 kW standby generator will provide power in the event of an electricity outage at the site. The generator is sized to have both pumps (duty and standby) running as well as power to station auxiliary equipment (lights, ventilation and controls) and an outdoor 30A receptacle for temporary pumps. The generator will automatically start upon a sustained outage in the permanent power supply. The automatic transfer switch will operate to connect the generator to the station equipment while disconnecting the permanent power supply. The 715 L double-walled diesel storage tank complete with low fuel sensor has sufficient capacity to allow the station to operate for 24 hours on standby power.

## 4.6 SUMMARY

The Fairgrounds SPS has been designed to service proposed residential development lands in the City of Stratford which are located at the old fairgrounds site and include an area of approximately 8.0ha for a peak design flow rate of 6.4 L/s. Based on the pump selection, the station's rated capacity will be 7.5 L/s. The system has been designed in accordance with the City of Stratford and the *MOE Design Guidelines for Sewage Works (2008)*. It should be noted that a Municipal Class EA, Schedule B will be required for a municipal pump station.

The Pump station will require an area of approximately 20mx20m and the preliminary cost estimate is \$1.08 million. This budget price includes the following items:

- Site preparation, grading & sediment control;
- Dewatering;
- Wet well & pumps;
- Generator building including instrumentation, controls and standby power generator;
- Electrical work;
- Mechanical work;
- Water service, storm sewers and sanitary sewers & forcemain within the pump station site limits; and
- Asphalt driveway, topsoil, sod, landscaping & fence.

The forcemain required to convey the flows from the pump station is a 100mm diameter. The approximate cost to install the forcemain from the proposed pump station to John and Charles Street is \$60,000. Refer to Figure 5 for the preliminary routing of the proposed forcemain.



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## 5.0 STORMWATER MANAGEMENT

## 5.1 Existing Stormwater Servicing

The predevelopment land use of the subject site consists of large buildings with parking lots, baseball diamonds and grassed areas. The predevelopment land use of the recreational facility lands north of the site was considered to be row crops, while the developed land west of the subject site was modeled as a subdivision for the predevelopment condition.

The stormwater flows from the south most area of the site outlet to the Britannia Street storm sewer while an area just north of this portion outlets to the storm sewer on Glastonbury Drive. The remaining north portion of the site outlets to the 1050mm diameter trunk storm sewer; which is located within the site. This sewer also services the 12.54 ha residential subdivision (Briarhill) to the west.

The 1050mm storm sewer enters the subject site approximately 360 meters north of Britannia Street within an existing pedestrian walkway and exits the site at the northeast corner of the property towards Warwick Road.

The current overland flow route enters the site from Briarhill Dr. near the south leg of both Windemere Cres. and Braemar Cres. The overland flow then travels towards the northeast corner of the site where it outlets towards Waddell St. The major drainage flow path for the site has been derived from Figure 5.3 'Existing System Screening (NW)' in the City of Stratford's *City-Wide Storm System Master Plan (October 2004)* prepared by Dillon Consulting.

Stormwater flows produced by the Rotary Recreational Facility north of the subject lands are directed to an existing dry pond which is located at the south end of the recreational site. The discharge from the dry pond is controlled by a 285mm diameter orifice which outlets to the existing 1050mm trunk storm sewer.

Refer to Figure 6 for illustration and clarification of the existing storm sewer servicing.



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## 5.2 SWM Design Criteria

The proposed development site will be required to control storm flows in accordance to the MOECC and City of Stratford guidelines. This developed site will be required to be provided with both SWM quantity and quality controls. The stormwater management design targets to minimize the impact of development on the downstream watercourse are identified in sections 5.2.1 and 5.2.2.

The proposed SWM facility is required to be designed to consolidate storm drainage from the proposed development site and the existing Rotary Complex north of the subject site. The SWM criteria noted above will also apply to the storm drainage from the Rotary Complex site.

The existing storm drainage from the external lands west of the subject property is to be conveyed through the SWM facility and not subject to quality or quantity controls.

## 5.2.1 Quality Control

The City of Stratford requires that stormwater quality control be provided to achieve a *Normal* level of protection, which would require a 70% long term suspended solid removal.

As outlined in the *Ministry of the Environment's Storm Water Management Planning and Design Manual*, a Wet Pond receiving drainage from an area that is 55% impervious with Normal protection requires storage of 110 m<sup>3</sup>/ha for water quality treatment. The required storage volume includes 70 m<sup>3</sup>/ha in the permanent pool (Dead Storage) and 40 m<sup>3</sup>/ha for extended detention (Active Storage for erosion control).

Additionally a Wet Pond receiving drainage from an area that is 95% impervious with Normal protection requires storage of 165 m<sup>3</sup>/ha for water quality treatment. The required storage volume includes 125 m<sup>3</sup>/ha in the permanent pool (Dead Storage) and 40 m<sup>3</sup>/ha for extended detention (Active Storage for erosion control).

## 5.2.2 Quantity Control

Stormwater Quantity Control is to be provided such that the post development 250 year storm event peak flow rates are restricted to the 5 year storm predevelopment level.

## 5.3 Predevelopment Condition

The predevelopment land use of the 12.68 ha area containing the subject site consists of large buildings with parking lots, baseball diamonds and grassed areas. The predevelopment land use of the 7.81ha recreational facility lands north of the site was considered to be row crops, while the 12.54 ha of developed land west of the subject site was modeled as a subdivision for predevelopment condition.

Refer to Figure 7 for the predevelopment catchment areas plan.

# 5.4 Proposed Stormwater Servicing Strategy

To accommodate the quality and quantity SWM criteria required, a wet pond has been proposed to service the subject site and the Rotary Complex. The drainage (minor and major flows) from the westerly external lands (Briarhill) will be conveyed through the proposed SWM facility but will not be subject to additional treatment. The SWM Block required to be allocated for the proposed SWM facility has been determined to be  $11,700 \text{ m}^2$  (1.17 ha).

The proposed SWM Facility will allow the existing dry SWM facility for the Rotary Complex site to be decommissioned. The minor and major storm flows are directed to the proposed SWM Facility through a swale along the west boundary of the subject site. The swale will include a ditch inlet catchbasin that outlets to the proposed SWM facility.

The existing 1050mm trunk storm sewer servicing the subdivision west of the site (Briarhill) is undersized and unable to convey the 5 year storm event. It is proposed to upsize approximately 50m of this sewer from the Briarhill subdivision and outlet this sewer to the proposed SWM facility. The SWM outlet and downstream storm sewers will convey the restricted flows from the proposed development lands and the conveyed flows from the Briarhill subdivision.

Both the inlet and outlet sewer construction will be required to be completed as part of the redevelopment of the fairground property. It should be noted that although the construction of these works will assist with some of the current deficiencies with the Briarhill storm sewer system, additional sewer replacement in the Briarhill subdivision will be required in the future to eliminate all capacity constraints.

Refer to Figures 8 for the conceptual storm sewer servicing.

All internal and external overland flows will be conveyed through the subject site and directed towards the proposed SWM pond. The existing overland flow routes entering the site from the existing development to the west must be maintained. The overland flows leaving the SWM facility will be directed along the current location of the existing overland flow route to Waddell Street.

Refer to Figures 9 for the post development catchment areas.





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## 5.4.1 Quality Control

To satisfy the Normal level of quality control for the subject site area of 11.89 ha at 55% impervious, a 110 m<sup>3</sup>/ha storage volume was taken from Table 3.2 of the MOE Manual. The quality control storage volume requires an extended detention volume of 476 m<sup>3</sup> and a permanent pool volume of 832 m<sup>3</sup>.

Stormwater flows will enter the SWM facility through a headwall into a sediment forebay. The forebay has been designed to be 15.0 m wide by 27.0 m long and be 1.1m deep. This will provide approximate quality volume of 506  $m^3$  which exceeds the required volume.

For the 7.13 ha of the recreational facility at 95% impervious, an interpolated storage volume of 165  $m^3$ /ha was calculated. The quality control storage volume requires an extended detention volume of 285  $m^3$  and a permanent pool volume of 892  $m^3$ .

Stormwater flows will enter the SWM facility through a headwall into a second sediment forebay. The forebay has been designed to be 13.0 m wide by 30.0 m long and be 1.1m deep. This will provide approximate quality volume of 530 m<sup>3</sup> which exceeds the required volume.

A permanent pool has been designed to have a maximum ponding depth of 1.1 meter, with 3:1 slopes and provides an approximate volume of 3,380, which exceeds the required volume of 1,724  $m^3$ .

Refer to Figure 10 for illustration and clarification.

## 5.4.2 Quantity Control

The proposed SWM facility has been sized to accommodate and control the 250 year post development flow to the 5 year pre development flow. A total active storage volume of approximately 20,450 m<sup>3</sup> is available within the pond. Embankment grading to obtain the required storage volume has been designed to have a maximum allowable slope of 3:1.

Flows for extended detention and flood control are discharged to the storm sewer from a multi-stage outlet comprised of a 375mm outlet pipe and a 900mm outlet pipe (Figure 10). The 375mm pipe controls discharge for extended detention and the 900mm pipe is set above the storage elevation for extended detention.



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Design	Pre-	F	Total			
Storm	Development (m3/s)	Uncontrolled (m3/s)	Inflow (m3/s)	Discharge (m3/s)	Storage (m3)*	Flow (m3/s)
5-year	2.174	-	-	-	-	2.174
5-year		0.188	2.567	0.537	7,260	0.558
250-year	-	0.614	6.991	1.988	18,165	2.073

The following table summarizes the stormwater flow at the SWM facility.

\* Not including permanent pool storage of 3,380 m<sup>3</sup>

See Appendix B for stormwater management calculations and modeling information.

## 5.5 Summary

The proposed 1.14 ha Stormwater Management Block has been designed to service the proposed residential development, existing recreational facility and the existing trunk storm sewer. The SWM Block has been adequately sized to construct a SWM Facility that will restrict post development peak flows to the 5 year predevelopment peak flow for the 250 year storm post development event.

The SWM Pond will also provide the 'Normal' level of water quality treatment required for the proposed development and recreational facility. The SWM Block has been designed in accordance with the City of Stratford and the *MOE Storm Water Management Planning and Design Manual (2003)*.

The preliminary cost to construct the SWM Pond is \$315,000. This budget price includes the following items:

- Site preparation, grading & sediment control;
- Earth excavation, headwalls & landscaping.

The preliminary cost for works external to the SWM Block is \$250,000. This budget price includes the following items:

- Decommissioning of the existing dry pond;
- Upsizing/installation of Storm sewers and appurtenances;
- LID Swale

The preliminary cost for works associated with the SWM Pond outlet pipe is \$204,000.

The trunk storm sewer from Briarhill Drive has been designed to be upgraded and intercepted by the SWM Pond. The trunk sewer upgrades resume after the outlet from the SWM Pond and extend out to Warwick Road.

Overland flow routes that enter and leave the site are to remain in their current locations and be accommodated by the proposed development. Any potential changes to overland flow routes will need to be confirmed during detailed design.

## 6.0 CONCLUSIONS AND RECOMMENDATIONS

MTE hereby recommends the adoption of this report as a Preliminary Servicing Report demonstrating the intent and feasibility of providing services for the proposed development as summarized below:

## Sanitary Servicing

Sanitary sewers for the proposed development will be directed to the proposed Fairgrounds Sanitary Pumping Station:

- The Fairgrounds SPS has been designed to service approximately 8.0ha proposed residential development.
- The Pump station will require an area of approximately 20mx20m and the proposed discharge location for the Fairgrounds SPS is an existing manhole at the intersection of John Street and Charles Street.
- The preliminary cost estimate to construct the Fairgrounds SPS and associated forcemain is \$1,140,000.

## Stormwater Management and Storm Servicing

The proposed 1.14 ha Stormwater Management Block is adequately sized to construct a SWM Facility that will restrict post development peak flows to the 5 year storm predevelopment peak flows for the 250 year storm post development event. The SWM Pond will also provide the 'Normal' level of water quality treatment required for the proposed development and recreational facility.

- By redirecting the stormwater drainage from the recreational facility to the proposed SWM pond the existing dry pond can be decommissioned and the land can be repurposed to suit the needs of the site.
- The proposed outlet for the SWM Pond is the existing trunk sewer at Warwick Road.
- The preliminary cost estimate to construct the SWM Pond and complete all other stormwater works is \$769,000.

All of which is respectfully submitted,

## MTE CONSULTANTS INC.

Jamie Dick, P. Eng. Design Engineer

Conceptual Servicing Report Stratford Fairgrounds

Bill Veitch, P. Eng. Director

![](_page_27_Picture_0.jpeg)

# **APPENDIX A**

# **Sewage Treatment Plant Preliminary Calculations**

# Conceptual Wastewater Pumping Station Design

Project Name: Stratford Fairgrounds Project Number: 37888-300 Location: Stratford, ON Date: October 24, 2014

![](_page_28_Picture_2.jpeg)

No.	Calculation Title							
1	Wet well sizing to ensure cycle time >or = 10 minutes							
	<u>Formula</u>							
		Mhoro						
	$T_{1Q_1}$	Vi=	Minimum	vet well volume ensuring a cycle time of of T1				
	$V_1 = \frac{1}{4}$	01=	Pump disch	arge				
			Cycle time	(10 minutes minimum per MOE Guidlines)				
	<u>Cacluation</u>							
	1.0 EA document flowrate			Notes:				
	Parameter	Value	Units					
	Q1 =	6.4	L/s					
	T1 =	10.0	min					
	V1 =	961.5	L	Volume required between Pump ON & Pump OFF				
	Wet Well Diameter =	1.8	m					
	Required Depth =	0.4	m	Depth based on required volume and wet well geometry				
	Ground Elev. =	360.5	mAMSL					
	Lowest Inlet Invert =	356.0	mAMSL					
		0.3	m					
	Control Spacing =	0.3	m					
	Sumn –	0.3	m					
	Total Wet Well Depth =	6.0	m					
	Wet Well Base Elev. =	354.5	mAMSL					
	Calculation by: NJD							
	Checked by:							
	Forcomain Pating Curve - Flowm	octor						
2	Torcemain Nating Curve - Howing							
	Parameter	Value	Units					
	Outlet Pressure	0	m H20					
	Pump Inlet Elevation	354.7	mAMSL					
	Forcemain High Point	359	mAMSL					
	Forcemain Length	450	m					
	Ftg Losses (Equiv. Length)	14.783	m					
	Roughness Coeff	404.783 120	n N/A					
	Forcemain Diameter	100	mm					
	Discharge	<u>6.4</u>	L/s					
			· · ·					
	F/M Velocity	0.82	m/s					
	Total Dynamic Head (TDH)	8.36	m H20					
	Static Head	4.3	m H20					

# **Stratford Fairground Sewage Pumping Station** Design Flowrate Calculation

## **Calculation Parameters**

		Per concept plan	Per max density
Total Residential Serv	icing Area (ha)	7.731	
Densitys (units/ ha)	R1	20	
	R2	30	
	R4	50	
	R5	100	
Total number of Units	5		check
R1 (28350	.3 m^2)	52	56.7
R2 (11026	.4 m^2)	28	33.1
R4 (11932	.1 m^2)	41	59.7
R5 (3624 r	m^2)	24	36.2
		145	185.7
Persons/ Unit		2.4	2.4
Total Population		348	446

Peak Factor (Harmon) (ave)		4.050	3.999
infiltration (I/s/ha)		0.1	0.1
Per Capita Flow Rate (I/s/pp)	0.004	345.6 (l/pp/day)	345.6

## **Peak Flow Calculation**

Q(peak) = (PqM/86.4)+IA						
Q (peak) = ((.348)(345.6)(	4.05)/86.4)+(.1)(7.73)					
Q(peak) =	6.41083 l/s	7.902103				

## **Average Flow Calculation**

Q(avg) = (PqM/86.4)+IA

Q (avg) = ((.348)(345.6)(1.0)/86.4)+(.1)(7.73)

$O(a_{1}a_{2})$		2 5 5 7
Q(avg) –	2.105 1/5	2.557

![](_page_30_Picture_0.jpeg)

# **APPENDIX B**

# Storm Water Management Preliminary Calculations

# STRATFORD FAIRGROUNDS STORMWATER MANAGEMENT

Stratford, Ontario

 Project Number:
 37888-300

 Date:
 December 5, 2014

 Design By:
 JMD

 File:
 Q:\37888\300\SWM Design\37888-300 Forebay Design\_Rev4.0.0.xls

## HYDROLOGIC PARAMETERS

### **Pre-Development Conditions**

![](_page_31_Picture_5.jpeg)

### **Post-Development Conditions**

Sub-Catchment	_	Percent	Impervious	Overland	Overland	SCS Curv	ve Number		
Number	Area	Impervious	Area	Slope	Length	Pervious	Impervious	Land Use	Comment
	(ha)	(%)	(ha)	(%)	( <i>m</i> )				
201	12.54	55	6.90	2.00	36	84	98	Residential	External Subdivision
202	7.13	95	6.77	0.50	60	84	98	Commercial	Recreational Facility
203	11.89	55	6.54	0.50	610	84	98	Residential	Future Development
204	0.79	55	0.43	2.00	36	84	98	Residential	Future Develop Uncontrolled
205	0.68	0	0.00	0.50	10	84	98	Commercial	Rec. Facility - Uncontrolled
Total	33.03	63	20.64						

![](_page_31_Picture_8.jpeg)

### STRATFORD FAIRGROUNDS STORMWATER MANAGEMENT Stratford, Ontario

Project Number:	37888-300
Date:	December 5, 2014
Design By:	JMD
File:	Q:\37888\300\SWM Design\37888-300 Forebay Design_Rev4.0.0.xls

#### FOREBAY DESIGN CALCULATIONS - Proposed Subdivision Outlet MOE SWM Planning and Design Manual, 2003

#### **Forebay Design Flows**

Flow into forebay during the 1:5-year return period event	1.00	m³/s
Flow into forebay during the 25 mm - 4 hour design storm event	0.37	m³/s
Peak flow from main pond outlet for the 25mm design storm (from MIDUSS)	0.148	m³/s

#### **Forebay Characteristics**

b =	15.0	т	bottom width
y =	1.1	т	depth
Z =	3	:1	side slope
w =	18.3	т	average width
R =	0.92	т	hydraulic radius
A =	20.1	m²	cross-sectional area

#### 1. Length Calculation Based on Settling Velocity

L = forebay flow length (m)

- r = length-to-width ratio
- $Q_p = peak$  flow rate through forebay  $(m^3/s)$
- $v_s =$  settling velocity (*m*/*s*)

 $L = \sqrt{\frac{rQ_p}{v_s}}$ 

Table 1: Average settling velocities

Mass

Removed

%

80 - 100

70 - 80

60 - 70

40 - 60

20 - 40

Equation 4.5: Forebay Settling Length

**Particle Size** 

Range

μm

x ≤ 20

 $20 < x \le 40$ 

 $40 < x \le 60$ 

60 < x ≤ 130 130 < x ≤ 400

0 - 20 400 < x ≤ 4000

Average

Settling

Velocity

m/s

0.00000254

0.00001300

0.00002540

0.00012700

0.00059267

0.00550333

a) Required Settling Length (assuming $Q_n = 10$ repay through-now $\alpha v_s = 0.0055$ m	a) F	a)
--	------	----

Q <sub>p</sub> =	0.37	m³/s	peak flow rate through forebay
$V_s =$	0.0055	m/s	settling velocity
r =	0.20		length-to-width ratio
L =	3.6	m	required settling length
L =	3.6	т	trial length

### b) Required Settling Length (assuming $Q_{p}$ = pond discharge & $\nu_{s}$ = 0.0003 m/s)

Q <sub>p</sub> =	0.148	m³/s	peak flow rate through forebay
$V_s =$	0.0003	m/s	settling velocity
r =	1.48		length-to-width ratio
L =	27.0	т	required settling length
L =	27	т	trial length

#### 2. Length Calculation Based on Flow Dispersion Length

Q =	1.00 <i>m<sup>3</sup>/s</i>	inlet flow rate	т
d =	1.1 <i>m</i>	depth of permanent pool in forebay	$L_D$
$V_{f} =$	0.50 <i>m/s</i>	desired velocity in forebay (typical value $\leq 0.50 \ m/s$ )	
L =	14.5 m	required length of dispersion	

# $L_D = \frac{8Q}{dV_f}$

Enhanced:

Medium Sand:

Gross Grit:

Normal:

Basic:

Equation 4.6: Dispersion Length

3. Required Forebay Length

27.0 m

L =

design length

![](_page_32_Picture_25.jpeg)

### STRATFORD FAIRGROUNDS STORMWATER MANAGEMENT Stratford, Ontario

 Project Number:
 37888-300

 Date:
 December 5, 2014

 Design By:
 JMD

 File:
 Q:\37888\300\SWM Design\37888-300 Forebay Design\_Rev4.0.0.xls

#### FOREBAY DESIGN CALCULATIONS - Recreational Complex Outlet MOE SWM Planning and Design Manual, 2003

#### **Forebay Design Flows**

Flow into forebay during the 1:5-year return period event	0.87	m³/s
Flow into forebay during the 25 mm - 4 hour design storm event	0.32	m³/s
Peak flow from main pond outlet for the 25mm design storm (from MIDUSS)	0.148	m³/s

#### **Forebay Characteristics**

b =	13.0	т	bottom width
y =	1.1	т	depth
z =	3	:1	side slope
w =	16.3	т	average width
R =	0.90	т	hydraulic radius
A =	17.9	m²	cross-sectional area

#### 1. Length Calculation Based on Settling Velocity

L = forebay flow length (m)

- r = length-to-width ratio
- $Q_p = peak$  flow rate through forebay  $(m^3/s)$
- $v_s =$  settling velocity (*m*/*s*)

 $L = \sqrt{\frac{rQ_p}{v_s}}$ 

Enhanced:

Equation 4.5: Forebay Settling Length

**Particle Size** 

Range

μm

x ≤ 20

20 < x ≤ 40

 $40 < x \le 60$ 

Average

Settling

Velocity

m/s

0.00000254

0.00001300

0.00002540

) Required Settling Length (assuming $Q_p$ = forebay through-flow & $v_s$ = 0.0055 m/s)	Table 1: Average settling velocities
---	--------------------------------------

Q <sub>p</sub> =	0.32	m³/s	peak flow rate through forebay
$V_s =$	0.0055	m/s	settling velocity
r =	0.21		length-to-width ratio
L =	3.5	т	required settling length
L =	3.5	т	trial length

#### b) Required Settling Length (assuming $Q_p$ = pond discharge & v<sub>s</sub> = 0.0003 m/s) $Q_p = 0.148 \ m^{3}/s$ peak flow rate through forebay

Q <sub>p</sub> =	0.148	III /S	peak flow rate through forebay
$V_s =$	0.0003	m/s	settling velocity
r =	1.84		length-to-width ratio
L =	30.1	т	required settling length
L =	30	т	trial length

#### 2. Length Calculation Based on Flow Dispersion Length

Q =	0.87 m³/s	inlet flow rate	T
d =	1.1 <i>m</i>	depth of permanent pool in forebay	$L_D$ :
$V_{f} =$	0.50 <i>m/s</i>	desired velocity in forebay (typical value $\leq 0.50 \text{ m/s}$ )	
L =	12.6 m	required length of dispersion	

### Normal: 60 - 70

Mass

Removed

%

80 - 100

70 - 80

Basic:40 - 60 $60 < x \le 130$ 0.00012700Medium Sand:20 - 40 $130 < x \le 400$ 0.00059267Gross Grit:0 - 20 $400 < x \le 4000$ 0.00550333

 $=\frac{8Q}{dV_f}$ 

Equation 4.6: Dispersion Length

3. Required Forebay Length

30.1 m

L =

design length

![](_page_33_Picture_27.jpeg)

Predevelopment Hydrologic Modelling

"			MIDUISS Output				\"
"			MIDUSS version		Ve	ersion 2.25	rev. 473"
"			MIDUSS created		Sunda	av. February	v 07. 2010"
"		10	Units used:			1,	ie METRIC"
"			Job folder:		Q:\37888\3	00\SWM Des:	ign\MIDUSS"
"			Output filename:		378	888-300 Pre	005Yr3.out"
"			Licensee name:				Admin"
"			Company				Microsoft"
	0.1		Date & Time last use	ed:	11/2	27/2014 at 3	3:22:38 PM"
	31	T11	ME PARAMETERS"				
		240 000	May Storm longth"				
"		1500 000	Max. Storm rength Max Hydrograph"				
"	32	1300.000 ST(	ORM Chicago storm"				
"	01	1	Chicago storm"				
"		875.105	Coefficient A"				
"		7.641	Constant B"				
"		0.762	Exponent C"				
"		0.400	Fraction R"				
"		240.000	Duration"				
		1.000	Time step multiplier	- 100 10			
		Maz	ximum intensity	122.12	28 mm/hr'	•	
		101	005bud Hudrograph	JZ.40	34 mm" Jacod in thic	filo <b>"</b>	
	33	CA	TCHMENT 101"	excension (	isea in chiis	s IIIe	
"	00	1	Triangular SCS"				
"		2	Proportional to %"				
"		1	SCS method"				
"		101	Briarhill Subdivisio	on"			
"		55.000	% Impervious"				
		12.540	Total Area"				
		36.000	Flow length"				
		2.000	Overland Slope"				
		36 000	Pervious Area"				
"		2 000	Pervious slope"				
"		6.897	Impervious Area"				
"		44.000	Impervious length"				
"		2.000	Impervious slope"				
"		0.250	Pervious Manning 'n'				
"		84.000	Pervious SCS Curve N	lo."			
		0.450	Pervious Runoff coef	ficient"			
		0.100	Pervious la/S coeffi	LCIENT"			
		4.838	Pervious Initial abs	straction"			
		98 000	Impervious SCS Curve	NO "			
"		0.884	Impervious Runoff co	pefficient"			
"		0.100	Impervious Ia/S coef	ficient"			
"		0.518	Impervious Initial a	abstraction'	,		
"			1.985 0.000	0.000	0.000 c	c.m/sec"	
"		Cat	tchment 101	Pervious	Impervious	Total Area	"
		Sui	rface Area	5.643	6.897	12.540	hectare"
		Tir	me of concentration	16.608	2.614	6./2/	minutes"
		I 11 Doc	me to Centrold	153.035	119.923	129.655	minutes"
		Ra. Ra:	infall volume	2961 67	3619 82	52.404 6581 50	
"		Ra	infall losses	28.884	6.092	16.348	mm"
"		Rui	noff depth	23.601	46.392	36.136	mm"
"		Rui	noff volume	1331.78	3199.65	4531.43	c.m"
"		Rui	noff coefficient	0.450	0.884	0.689	"
"		Maz	ximum flow	0.440	1.883	1.985	c.m/sec"
"	40	HYI	DROGRAPH Add Runoff '	1			
"		4	Add Runoff "				
"	E 1		1.985 1.985	0.000	0.000"		
	ЪТ	1 0.0E	Current neek flow	a m/aca"			
"		1.900	Manning 'n'"	C.m/sec			
"		1.050	Diameter metre"				
"		0.070	Gradient %"				

" Surcharged HGL 0.528 <u>्</u>र ॥ ... m/sec" Velocity 2.292 0.722 c.m/sec" ... Pipe capacity ... Critical depth 0.000 metre" **"** 53 ROUTE Pipe Route 94" 94.00 Pipe Route 94 Reach length (metre)" 0.000 X-factor <= 0.5" ... ... X-factor <= 0.5" 0.000 K-lag (seconds)" ... ... 0.000 Default(0) or user spec.(1) values used" " 0.500 X-factor <= 0.5" 30.000 K-lag (seconds)" 0.000 Beta weighting factor" 0.000 Routing time step (seconds)" 0 No. of sub-reaches" " ... ... ... Peak outflow 1.985 c.m/sec" " 1.985 1.985 1.985 0.000 c.m/sec" **"** 40 HYDROGRAPH Next link " 5 Next link " 1.985 1.985 1.985 0.000" " 33 CATCHMENT 102" ... 1 Triangular SCS" ... 2 Proportional to %" 1 SCS method" 102 Future Development" ... ... 45.000 % Impervious" " ... 12.680 Total Area" ... 610.000 Flow length" 0.120 Overland Slope" 6.974 Pervious Area" 610.000 Pervious length" " ... " ... 0.120 Pervious slope" ... 5.706 Impervious Area" " 499.091 Impervious length" ... 0.120 Impervious slope" 0.250 Pervious Manning 'n'" ... 84.000 Pervious SCS Curve No." " " 0.450 Pervious Runoff coefficient" ... 0.100 Pervious Ia/S coefficient" ... 4.838 Pervious Initial abstraction" " 0.015 Impervious Manning 'n'" 98.000 Impervious SCS Curve No." " ... 0.900 Impervious Runoff coefficient" ... 0.100 Impervious Ia/S coefficient" ... 0.518 Impervious Initial abstraction" ... 0.000 c.m/sec" 0.763 1.985 1.985 

 0.763
 1.985
 1.985
 0.000 c.m/sec"

 Catchment 102
 Pervious
 Impervious Total Area
 "

 Surface Area
 6.974
 5.706
 12.680
 hectare"

 Time of concentration
 211.001
 26.101
 96.247
 minutes"

 Time to Centroid
 430.157
 155.989
 260.002
 minutes"

 Rainfall depth
 52.484
 52.484
 52.484
 mm"

 Rainfall volume
 3660.24
 2994.74
 6654.98
 c.m"

 Rainfall losses
 28.865
 5.260
 18.243
 mm"

 Runoff depth
 23.619
 47.224
 34.241
 mm"

 Runoff coefficient
 0.450
 0.900
 0.652
 "

 Maximum flow
 0.070
 0.753
 0.763
 c.m/sec"

 ... ... ... " ... ... ... " " ... HYDROGRAPH Add Runoff " 40 ... 4 Add Runoff " ... 0.763 2.173 1.985 0.000" **"** 51 PIPE DESIGN" 2.173 Current peak flow c.m/sec" 0.013 Manning 'n'" ... ... Manning 'n'" 1.050 Diameter metre" ... 0.110 Gradient %" ... ... <u>ي</u> اا Surcharged HGL 0.633 " 2.510 Velocity m/sec" 0.000 mot ... Pipe capacity Critical depth **"** 53 ROUTE Pipe Route 92"

" 92.00 Pipe Route 92 Reach length ( metre)" 0.000 X-factor <= 0.5" ... ... 0.000 K-lag (seconds)" ... 0.000 Default(0) or user spec.(1) values used" " 0.500 X-factor <= 0.5" 30.000 K-lag (seconds)" 0.000 Beta weighting fact " ... Beta weighting factor" 0.000 Routing time step ( seconds)" 0 No. of sub-reaches" ... ... " Peak outflow 2.173 c.m/sec" 2.173 " 0.763 2.173 0.000 c.m/sec" " 40 HYDROGRAPH Combine 1" 6 Combine " ... Node #" 1 ... ... " c.m/sec" Maximum flow 2.173 8873.207 " Hydrograph volume c.m" ... 0.763 2.173 2.173 2.173" ... HYDROGRAPH Start - New Tributary" 40 2 Start - New Tributary" ... ... 0.763 0.000 2.173 2.173" " 33 CATCHMENT 103" ... 1 Triangular SCS" ... 2 Proportional to %" ... SCS method" 1 ... 103 Fair Grounds" ... 0.000 % Impervious" 7.810 Total Area" 187.000 Flow length " ... Flow length" 1.500 Overland Slope" " ... 7.810 Pervious Area" ... 187.000 Pervious length" " 1.500 Pervious slope" ... 0.000 Impervious Area" 0.000 Impervious lengt ... Impervious length" 1.500 Impervious slope" " ... 0.250 Pervious Manning 'n'" ... 84.000 Pervious SCS Curve No." 0.450 Pervious Runoff coefficient" 0.100 Pervious Ia/S coefficient" ... " Pervious Ia/S coefficient" 4.838 Pervious Initial abstraction" " ... 0.015 Impervious Manning 'n'" ... 98.000 Impervious SCS Curve No." " 0.000 Impervious Runoff coefficient" 0.100 Impervious Ia/S coefficient" 0.518 Impervious Initial abstraction " 0.518 Impervious Initial abstraction" 0.276 0.000 2.173 ... 2.173 c.m/sec" ... Catchment 103 Pervious Impervious Total Area " ... 7.810 0.000 7.810 hectare" Surface Area 48.6540.002198.909115.32252.48452.484 minutes" " Time of concentration 48.654 48.654 Time to Centroid 198.909 52.484 198.909 ... minutes" ... 52.484 mm" ... 4099.00 0.00 Rainfall volume 4099.00 c.m" " 28.846 mm" Rainfall losses 28.846 9.981 Runoff depth 42.503 " 23.638 23.638 mm" Runoff volume Runoff coefficient 1846.120.000.4500.0000.2760.000 ... 1846.12 c.m" 0.450 0.276 0.450 ... Maximum flow c.m/sec" **"** 40 HYDROGRAPH Add Runoff " ... 4 Add Runoff " ... 0.276 2.173 2.173" 0.276 **"** 52 CHANNEL DESIGN" ... 0.276 Current peak flow c.m/sec" ... 0.025 Manning 'n'" " 0. Cross-section type: 0=trapezoidal; 1=general" 1.000 Basewidth metre" 50.000 Left bank slope" 50.000 Right bank slope" " " 0.300 Channel depth metre"

"		0.500 Gradient %"			
"		Depth of flow	0.105	metre"	
"		Velocity	0.420	m/sec"	
"		Channel capacity	3.914	c.m/sec"	
"		Critical depth	0 082	metre"	
"	53	POUTE Chappel Pou	to 340"	meere	
"	55	240 00 Chappel Boute	240 Boach longth	(motro)"	
		0.475 V faster ( 0.5"	540 Reach Tengch	( metre)	
		0.475 X-lactor <= $0.5$	. <b></b>		
		303.909 K-lag (seconds	)"		
		0.000 Default(0) or use	r spec.(1) values	used"	
		0.500 X-factor <= $0.5"$			
"		30.000 K-lag (seconds	)"		
"		0.500 Beta weighting fa	ctor"		
"		300.000 Routing time step	( seconds)"		
"		2 No. of sub-reache	s"		
"		Peak outflow	0.276	c.m/sec"	
"		0.276 0.	276 0.276	2.173 c.m/sec'	II
"	40	HYDROGRAPH Combine	1"		
"		6 Combine "			
"		1 Node #"			
"		"			
"		Maximum flow	2 174	a m/soa"	
		Hadrograph welume	10710 226	c.m/sec	
			276 0 276	0.174	
	10	U.276 U.	2/6 0.2/6	2.1/4"	
	40	HIDROGRAPH CONILUE	nce 1"		
		/ Confluence "			
		1 Node #"			
"		"			
"		Maximum flow	2.174	c.m/sec"	
"		Hydrograph volume	10719.335	c.m"	
"		0.276 2.	174 0.276	0.000"	
"	51	PIPE DESIGN"			
"		2.174 Current peak flow	c.m/sec"		
"		0.013 Manning 'n'"			
"		1.050 Diameter metre	"		
"		0.250 Gradient %"			
"		Surcharged HGL	0.634	s¦.∎	
"		Velocity	2.511	m/sec"	
"		Pipe capacity	1 365	c m/sec"	
"		Critical depth	0.000	metre"	
"	53	ROUTE Pipe Route	47 <b>"</b>	INCUIC	
"	55	47 00 Pine Route 47	-, Reach length ( m	netre)"	
"		47.00 Tipe Rouce $47$	Reach rengen ( n		
		202 000 K lag ( accords	х <b>п</b>		
		303.909 K-lag (seconds	)		
		0.000 Default(0) or use	r spec.(1) values	usea"	
		0.500 X - factor <= 0.5"			
		30.000 K-lag (seconds	)		
		0.500 Beta weighting fa	ctor"		
"		300.000 Routing time step	( seconds)"		
"		2 No. of sub-reache	s"		
"		Peak outflow	2.174	c.m/sec"	
"		0.276 2.	174 2.174	0.000 c.m/sec'	II
"	38	START/RE-START TOTAL	s 1"		
"		3 Runoff Totals on	EXIT"		
"		Total Catchment area		33.030	hectare"
"		Total Impervious are	a	12.603	hectare"
"		Total % impervious		38,156"	· · · · · · · · ·
"	19	EXIT"			

Post Development Hydrologic Modelling

"			MIDUSS Outpu	ıt				>"
"			MIDUSS versi	on		V	ersion 2.25	rev. 473"
"			MIDUSS creat	ed		Sund	av, Februar	v 07, 2010"
"		10	Units used:					ie METRIC"
"		10	Job folder:			0.137888	300\SWM Des	ian\MIDUSS"
"			Output filor	amo.		2. (37000 (	888-300 Pc+	005Vr2 out "
"			Liconcoo nom			51	000-300 FSC	Ndmin"
			Company					Miaroaoft"
			Doto ( Time	last use	ad.	10	/2/2014 -+	2.EE.40 DM
	2.1	<b>T</b> T	Dale & IIme	last use	30:	12	/2/2014 al	3:55:48 PM"
	31	E 000	ME PARAMEIERS	,				
		5.000	Time Step"					
		240.000	Max. Storm 1	.ength"				
"		1500.000	Max. Hydrogr	aph"				
"	32	ST	ORM Chicago s	storm"				
"		1	Chicago stor	.'m"				
"		875.105	Coefficient	A"				
"		7.641	Constant B"					
"		0.762	Exponent C"					
"		0.400	Fraction R"					
"		240.000	Duration"					
"		1.000	Time step mu	ltiplie	c"			
"		Ma	ximum intensi	ty	122.12	28 mm/hr	n	
"		То	tal depth	7	52.48	34 mm."		
"		6	005hvd Hvd	lrograph	extension 1	used in this	s file"	
"	33	ĊA	TCHMENT 201"	ir o gr apii	01100110101		0 1110	
"	00	1	Triangular S	3CS"				
"		2	Proportional	+0 %"				
"		1	SCS method"					
"		201	DDIADUTII CI					
		55 000	& Importious	, H	JIN			
		12 540	~ Impervious	,				
		12.040	Flour longth	,				
		30.000	FIOW LENGLIN					
		2.000	Overland Sic	pe" "				
		5.643	Pervious Are	a"				
		36.000	Pervious ler	igth"				
		2.000	Pervious slo	pe"				
"		6.897	Impervious A	irea"				
"		44.000	Impervious l	.ength"				
"		2.000	Impervious s	;lope"				
"		0.250	Pervious Mar	ning 'n'				
"		84.000	Pervious SCS	Curve N	No."			
"		0.450	Pervious Run	off coef	fficient"			
"		0.100	Pervious Ia/	'S coeffi	icient"			
"		4.838	Pervious Ini	tial abs	straction"			
"		0.015	Impervious M	lanning '	'n'"			
"		98.000	Impervious S	SCS Curve	e No."			
"		0.884	Impervious F	≀unoff co	pefficient"			
"		0.100	Impervious I	ia/S coef	fficient"			
"		0.518	Impervious I	nitial a	abstraction'	•		
"			1.985	0.000	0.000	0.000	c.m/sec"	
"		Ca	tchment 201		Pervious	Impervious	Total Area	
"		Su	rface Area		5.643	6.897	12.540	hectare"
"		Ti	me of concent	ration	16 608	2 614	6 727	minutes"
"		Ti	me to Centroi	d	153 035	119 923	129 655	minutes"
"		Ra	infall denth	.u	52 484	52 484	52 484	mm"
"		Ra	infall volume	2	2961 67	3619 82	6581 50	
		Ra Pa	infall loccos	;	2901.07	6 092	16 3/8	mm"
		Na Du	noff donth	,	20.004	16 202	26 126	mm "
		Ru	norr depth		ムン・UUL 1001 70	70.372 2100 CF	JU.LJU 4521 42	
		Ru	NOLL VOLUME	ont	1331./X	2133.02	4331.43	C.m
		Ru	HULL COEIIICI	.ent	0.430	U.004 1 002	U.009 1 005	
	4.0	Ma	XIMUM IIOW	D	U.44U	1.003	1.985	c.m/sec"
	40	HY	DRUGRAPH Add	KUNOII				
		4	Add Runoff "					
	5.6		1.985	1.985	0.000	0.000"		
	51	PI	PE DESIGN"		, -			
		1.985	Current peak	flow	c.m/sec"			
		0.013	Manning 'n'"					
		1.200	Diameter	metre"				
"		0.300	Gradient %	; "				

" Depth of flow 0.915 metre" ... Velocity 2.145 m/sec" 2.135 c.m/sec" ... Pipe capacity ... Critical depth 0.775 metre" **"** 53 ROUTE Pipe Route 60" 60.00 Pipe Route 60 Reach length ( metre)" 0.000 X-factor <= 0.5" ... ... X-factor <= 0.5" 20.984 K-lag (seconds)" ... ... 0.000 Default(0) or user spec.(1) values used" " 0.500 X-factor <= 0.5" 30.000 K-lag (seconds)" 0.856 Beta weighting factor" 100.000 Routing time step (seconds)" 1 No. of sub-reaches" " ... ... ... Peak outflow 1.910 c.m/sec" " 1.985 1.985 1.910 0.000 c.m/sec" **"** 40 HYDROGRAPH Combine 1" 6 Combine " ... 1 Node #" ... SWM POND" " Maximum flow 1.910 c.m/sec" Hydrograph volume ... Hydrograph volume 4531.426 1.985 1.985 1.910 HYDROGRAPH Start - New Tributary" c.m" ... 1.910" **"** 40 ... 2 Start - New Tributary" 0.000 ... 1.985 1.910 1.910" " 33 CATCHMENT 202" 1 Triangular SCS"
2 Proportional to %"
1 SCS method" ... ... " ... 202 Fair Grounds" ... 95.000 % Impervious" 7.130 Total Area" 60.000 Flow length" 0.500 Overland Slope" " ... ... 0.357 Pervious Area" " " 60.000 Pervious length" ... 0.500 Pervious slope" 6.773 Impervious Area" 1140.000 Impervious length" 0.500 Impervious slope" ... " " ... 0.250 Pervious Manning 'n'" " 84.000 Pervious SCS Curve No." 0.450 Pervious Runoff coefficient"
0.100 Pervious Ia/S coefficient"
4.838 Pervious Initial abstraction"
0.015 Impervious Manning 'n'" " " ... ... ... 98.000 Impervious SCS Curve No." ... 0.900 Impervious Runoff coefficient" 0.100 Impervious Ia/S coefficient" 0.518 Impervious Initial abstraction" " ... ... 0.875 0.000 1.910 1.910 c.m/sec" 

 0.875
 0.000
 1.910
 1.910 c.m/sec"

 Catchment 202
 Pervious
 Impervious Total Area
 "

 Surface Area
 0.357
 6.773
 7.130
 hectare"

 Time of concentration
 34.201
 27.922
 28.083
 minutes"

 Time to Centroid
 178.206
 158.786
 159.284
 minutes"

 Rainfall depth
 52.484
 52.484
 52.484
 mm"

 Rainfall volume
 187.11
 3555.01
 3742.11
 c.m"

 Rainfall losses
 28.853
 5.258
 6.438
 mm"

 Runoff depth
 23.631
 47.226
 46.046
 mm"

 Runoff coefficient
 0.450
 0.900
 0.877
 "

 Maximum flow
 0.017
 0.859
 0.875
 c.m/sec"

 ... " " ... ... ... " " ... c.m/sec" ... **"** 40 HYDROGRAPH Add Runoff " ... 4 Add Runoff " " 0.875 0.875 1.910 1.910" " 52 CHANNEL DESIGN" 0.875 Current peak flow c.m/sec" 0.040 Manning 'n'"

```
0. Cross-section type: 0=trapezoidal; 1=general"
3.000 Basewidth metre"
"
...
...
             3.000 Left bank slope"
...
             3.000 Right bank slope"
"
             0.750 Channel depth metre"
"
             0.500 Gradient %"
...
                     Depth of flow
                                                                     0.316
                                                                                  metre"
...
                                                                    0.701 m/sec"
                     Velocity
...
                     Channel capacity
                                                                     4.434 c.m/sec"
...
                     Critical depth
                                                                     0.192 metre"
" 53
                    ROUTE Channel Route 250"
            250.00 Channel Route 250 Reach length ( metre)"
0.430 X-factor <= 0.5"
...
...
...
          267.494 K-lag (seconds)"
...
            0.000 Default(0) or user spec.(1) values used"
"
             0.500 X-factor <= 0.5"
          30.000 K-lag (seconds)"
0.500 Beta weighting factor"
300.000 Routing time step (seconds)"
1 No. of sub-reaches"
...
...
...
...

        Peak outflow
        0.869
        c.m/sec"

        0.875
        0.875
        0.869
        1.910
        c.m/sec"

"
"
" 40
                     HYDROGRAPH Combine 1"
                    6 Combine "
...
                       Node #"
                    1
...
                         SWM POND"
                               2.005
7814.511
0.875 0.875 0.860
RAPH Start - Y
...
                     Maximum flow
                                                                                c.m/sec"
                     Hydrograph volume
"
                                                                                  c.m"
...
                                                                                 2.005"
                     HYDROGRAPH Start - New Tributary"
  40
                    2 Start - New Tributary"
...
...
                                0.875 0.000
                                                               0.869 2.005"
" 33
                    CATCHMENT 203"
                    1 Triangular SCS"
2 Proportional to %"
...
"
                   1 SCS method"
...
                 203 Future Development"
...
           55.000 % Impervious"
          11.890 Total Area"
610.000 Flow length"
...
"
            0.500 Overland Slope"
"
...
             5.351 Pervious Area"
"
          610.000 Pervious length"
"
            0.500 Pervious slope"
"
          6.540 Impervious Area"
745.556 Impervious lengt
...
                          Impervious length"
            0.500 Impervious slope"
...
...
            0.250 Pervious Manning 'n'"
...
           84.000 Pervious SCS Curve No."
            0.450 Pervious Runoff coefficient"0.100 Pervious Ia/S coefficient"4.838 Pervious Initial abstraction"
"
...
...
...
            0.015 Impervious Manning 'n'"
"
            98.000 Impervious SCS Curve No."
            0.900 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
0.518 Impervious Initial abstraction
"
...
                          Impervious Initial abstraction"
...
                               1.022 0.000 0.869
                                                                                2.005 c.m/sec"
                                            Pervious Impervious Total Area "
...
                     Catchment 203

      Surface Area
      5.351
      6.540
      11.890
      hectare"

      Time of concentration
      137.514
      21.642
      55.307
      minutes"

      Time to Centroid
      326.005
      149.140
      200.526
      minutes"

      Rainfall depth
      52.484
      52.484
      52.484
      mm"

"
"
...
...

        Rainfall volume
        2808.16
        3432.19

        Dainfall volume
        2808.16
        3432.19

...
                                                                                         6240.35
                                                                                                             c.m"
                                                       28.848 5.261
...
                                                                                          15.875 mm"
                     Rainfall losses

      Runoff depth
      23.636
      47.223
      36.609
      mm"

      Runoff volume
      1264.66
      3088.12
      4352.78
      c.m"

      Runoff coefficient
      0.450
      0.900
      0.698
      "

      Maximum flow
      0.079
      1.009
      1.022
      c.m/sec"

"
...
```

"	40	HY	DROGRAPH Add	d Runoff	"		
		4	Add Runoff	"			0.005
	F 0		1.022	1.02	22 0.	869	2.005"
	52	1 022	ANNEL DESIG	N" al flou	a m/aa	~"	
		1.022	Manning In	ak liow	C.m/se	C	
"		0.015	Cross-sect:	ion type	• O-trane	zoidal•	1-general"
"		2 000	Basewidth	metre'	. 0-trape "	201041,	I-general
"		50 000	Left bank	slope"			
"		50.000	Right bank	slope"			
"		0.300	Channel de	oth me	etre"		
"		0.500	Gradient	8 <b>"</b>			
"		De	pth of flow			0.136	metre"
"		Ve	locity			0.852	m/sec"
"		Ch	annel capac:	ity		7.066	c.m/sec"
"		Cr	itical dept	h		0.135	metre"
"	53	RC	OUTE Chani	nel Route	e 50"		
"		50.00	Channel	Route 50	) Reach l	ength	( metre)"
		0.385	X-factor <=	= 0.5"			
		44.026	K-lag (:	seconds)			
		0.000	Default(0)	or user	spec.(1)	values	used"
		20.000	X-lactor <=	= 0.5			
		50.000	R-Iay (: Pota wojah	seconds) ting fact	"		
"		50 000	Bela wergin Routing tir	ne sten	( secon	ds)"	
"		1	No of sub-	-reaches	"	u.5 /	
"		Pe	ak outflow	reaction		1.002	c.m/sec"
"			1.022	1.02	22 1.	002	2.005 c.m/sec"
"	40	HY	DROGRAPH (	Combine	1"		
"		6	Combine "				
"		1	Node #"				
"			SWM POND"				
"		Ma	ximum flow	_		2.567	c.m/sec"
		Ну	drograph vol	lume	1216	7.296	c.m"
	10	113		I.U. Confluon		002	2.56/"
"	40	7	Confluence	"	Je I		
"		, 1	Node #"				
"		1	SWM POND"				
"		Ma	ximum flow			2.567	c.m/sec"
"		Hy	drograph vo	lume	1216	7.297	c.m"
"		-	1.022	2.50	57 1.	002	0.000"
"	54	PC	ND DESIGN"				
"		2.567	Current pea	ak flow	c.m/se	с"	
"		2.000	Target out:	flow (	c.m/sec"		
		12167.3	Hydrograph	volume	c.m"		
		100 000	Number of :	stages"			
		102.000	Manimum wa	ter leve.	L metr	e" o <b>"</b>	
"		100.000	Starting Wa	ater leve	al met	e ro <b>"</b>	
"		100.000	Keep Design	n Data:	l = True:	0 = Fa	lse"
"		0	Level Di	scharge	Volume	"	100
"			100.000	0.000	0.000	"	
"			100.200	0.02045	1074.207	"	
"			100.400	0.06830	2187.288	"	
"			100.600	0.1209	3339.734	"	
"			100.800	0.1986	4532.208	"	
"			101.000	0.3288	5765.196	"	
"			101.200	0.5024	7039.318		
			101.400	0.7069	8355.202		
			LUL.600	0.9282	9/13.323		
			102 000	1 202	12550 70		
			102.000	1.303 1.550	1/0/7 22	"	
"			102.200	1 735	15580 31	"	
"			102 600	1 896	17158 50	"	
"			102.800	2.045	18782.50	"	
"			103.000	2.183	20452.76	"	
"		1.	LAYERS"				

"	Bottom	Aspect	Bottom	Тор	Average"	
"	area	ratio	elevation e	elevation	sideslope"	
"	5275.000	2.400	100.000	103.000	3.000"	
	2. OUTFLOW	PIPE"	D	D.'	Ma	<b>D</b>
	Upstream	Downstr'm	Pipe	Pipe	Manning	Entry"
	100 000	99 700	Length	Diameter 0 375	0 013	1055 Ke" 0 500 <b>"</b>
"	100.600	100 300	30,000	0.970	0.013	0.500"
"	Peak outfl	200 <b>.</b> 000	0.	.537 c.	.m/sec"	0.000
"	Maximum le	vel	101.	.234 me	etre"	
"	Maximum st	orage	7260.	.573 с.	. m "	
"	Centroidal	lag	8.	.991 hou	ırs"	
"	1.022	2.567	0.537	0.000	c.m/sec"	
	40 HYDROGRAPH	Next link	"			
	5 Next 11	nk" ∩>> ∩⊑	27 0 51	27 0 0	00"	
"	33 CATCHMENT	022 0.5 204"	0.5	57 0.0	000	
"	1 Triangu	lar SCS"				
"	2 Proport	ional to %"				
"	1 SCS met	hod"				
"	204 Future	Development	"			
"	55.000 % Imper	vious"				
	0.790 Total A	rea"				
	36.000 Flow les	ngth" d Clama <b>"</b>				
	0.356 Porviou	a Siope" s Aroa"				
"	36.000 Perviou	s length"				
"	2.000 Perviou	s slope"				
"	0.435 Impervi	ous Area"				
"	44.000 Impervi	ous length"				
"	2.000 Impervi	ous slope"				
	0.250 Perviou	s Manning '	n'"			
	84.000 Perviou	s SCS Curve	NO."			
	0.450 Perviou	s Runoll CC s Ta/S coef	ficient"			
"	4.838 Perviou	s Initial a	bstraction'	•		
"	0.015 Impervi	ous Manninc	'n'"			
"	98.000 Impervi	ous SCS Cur	ve No."			
"	0.884 Impervi	ous Runoff	coefficient	_ "		
	0.100 Impervi	ous Ia/S co	efficient"	_		
	0.518 Impervi	ous Initial	abstractio	on"		
	Catabrant .	125 0.5	0.53 Doruioud	J U.U	JUU C.M/SeC"	
"	Surface Ar	204	0 356	0 435	0 790	hectare"
"	Time of co	ncentratior	16.608	2.614	6.727	minutes"
"	Time to Ce	ntroid	153.036	119.923	129.655	minutes"
"	Rainfall d	epth	52.484	52.484	52.484	mm "
"	Rainfall v	olume	186.58	228.04	414.62	c.m"
	Rainfall l	osses	28.884	6.092	16.348	mm "
	Runoii dep	th	23.601	46.392	36.136	mm "
	RUNOII VOI Bunoff coe	ulle fficient	0 450	201.57	203.47	"
"	Maximum fl	OW	0.028	0.119	0.125	c.m/sec"
"	40 HYDROGRAPH	Add Runoff	"	0.110	0.120	0.111, 0000
"	4 Add Run	off "				
"	0.	125 0.5	47 0.53	37 0.0	000"	
"	52 CHANNEL DE	SIGN"				
"	0.547 Current	peak flow	c.m/sec'			
"	0.015 Manning	'n'"				
	U. Cross-s	ection type	: u=trapezo	j = 0	jeneral"	
"	50 000 Left bar	un metre nkslope"	:			
"	50.000 Right h	ank slope"				
"	0.300 Channel	depth m	letre"			
"	0.500 Gradien	t %"				
"	Depth of f	low	0.	.070 me	etre"	
"	Velocity		0.	.673 m/	sec"	
	Channel ca	pacity	10.	.429 c.	.m/sec"	
	Critical d	eptn	0.	.06/ me	etre"	

```
" 53
              ROUTE Channel Route 170"
          170.00 Channel Route 170 Reach length (metre)"
...
           0.478 X-factor <= 0.5"
...
          189.367 K-lag (seconds)"
"
           0.000 Default(0) or user spec.(1) values used"
           0.500 X-factor <= 0.5"
30.000 K-lag (second
"
...
                        K-lag (seconds)"
            0.500 Beta weighting factor"
...
         150.000 Routing time step ( seconds)"
1 No. of sub-reaches"
...
...
                                             0.547 c.m/sec"
0.547 0.547 0.000 c.m/sec"
"
                   Peak outflow
...
                                0.125
                  HYDROGRAPH Combine 2"
6 Combine "
" 40
...
...
                   2 Node #"
"
                                                                           c.m/sec"
"
                   Maximum flow
                                                               0.547

        Maximum flow
        0.547

        Hydrograph volume
        11625.695

        0.125
        0.547

...
                                                                             c.m"
...
                                                                           0.547"
" 40
                   HYDROGRAPH Start - New Tributary"
...
                  2 Start - New Tributary"
"
                                           0.000
                                                            0.547 0.547"
                              0.125
" 33
                   CATCHMENT 205"
                  1 Triangular SCS"
...
                  2 Proportional to %"
...
                  1
                      SCS method"
...
                205 Fair Grounds - Uncontrolled"
           0.000 % Impervious"
0.680 Total Area"
"
...
           10.000 Flow length"
"
...
           0.500 Overland Slope"
...
           0.680 Pervious Area"
"
           10.000 Pervious length"
...
           0.500 Pervious slope"
...
                        Impervious Area"
            0.000
            0.000 Impervious length"
"
"
           0.500 Impervious slope"
...
            0.250 Pervious Manning 'n'"
           84.000 Pervious SCS Curve No."
0.450 Pervious Runoff coefficien
0.100 Pervious Ia/S coefficient"
...
"
                        Pervious Runoff coefficient"
"
...
           4.838 Pervious Initial abstraction"
"
            0.015 Impervious Manning 'n'"
"
           98.000 Impervious SCS Curve No."
...
            0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
...
            0.518 Impervious Initial abstraction"
...
...
                             0.063 0.000 0.547
                                                                         0.547 c.m/sec"
...
                    Catchment 205 Pervious Impervious Total Area "

      Catchment 205
      Pervious
      Impervious
      Total Area
      "

      Surface Area
      0.680
      0.000
      0.680
      hectare"

      Time of concentration
      11.672
      0.000
      11.672
      minutes"

      Time to Centroid
      145.915
      115.326
      145.915
      minutes"

      Rainfall depth
      52.484
      52.484
      52.484
      mm"

      Rainfall volume
      356.89
      0.00
      356.89
      c.m"

      Runoff depth
      23.621
      42.521
      23.621
      mm"

      Runoff volume
      160.62
      0.000
      160.62
      c.m"

"
...
...
...
"
"
...
                                                                                                   "
...
                                                                   0.000
                                                                                     0.450
                   Runoff coefficient
                                                    0.450
                                                     0.063
...
                                                                   0.000
                                                                                    0.063 c.m/sec"
                   Maximum flow
" 40
                  HYDROGRAPH Add Runoff "
"
                  4 Add Runoff "
...
                                              0.063 0.547
                               0.063
                                                                         0.547"
" 52
                   CHANNEL DESIGN"
...
             0.063 Current peak flow c.m/sec"
...
             0.040 Manning 'n'"
                0. Cross-section type: 0=trapezoidal; 1=general"
"
           0.000 Basewidth met
50.000 Left bank slope"
"
                       Basewidth metre"
...
           50.000 Right bank slope"
```

"	0.300	Channel depth	metre"			
"	0.500	Gradient %"				
"	De	pth of flow		0.079	metre"	
"	Ve	locity		0.204	m/sec"	
"	Ch	annel capacity		2.245	c.m/sec"	
"	Cr	itical depth		0.050	metre"	
"	53 RO	UTE Channel Rou	ite 360"			
"	360.00	Channel Route	360 Reach	length	( metre)"	
"	0.459	X-factor <= 0.5"		-		
"	264.418	K-lag (seconds	s) <b>"</b>			
"	0.000	Default(0) or use	er spec.(1)	values u	used"	
"	0.500	X-factor <= 0.5"	-			
"	30.000	K-lag (seconds	s) <b>"</b>			
"	0.500	Beta weighting fa	actor"			
"	300.000	Routing time step	o (secor	nds)"		
"	5	No. of sub-reache	es"			
"	Pe	ak outflow		0.059	c.m/sec"	
"		0.063 0.	.063 0.	059 (	0.547 c.m/sec	
"	40 HY	DROGRAPH Combine	e 2"			
"	6	Combine "				
"	2	Node #"				
"		"				
"	Ma	ximum flow		0.558	c.m/sec"	
"	Hy	drograph volume	1178	36.317	c.m"	
"		0.063 0.	.063 0.	059 (	).558"	
"	38 ST	ART/RE-START TOTAL	LS 205"			
"	3	Runoff Totals on	EXIT"			
"	То	tal Catchment area	a		33.030	hectare"
"	То	tal Impervious are	ea		20.644	hectare"
"	То	tal % impervious			62.502"	
"	19 EX	IT"				

"			MIDUSS Outr	out						>
"			MIDUSS vers	sion				Ver	sion 2.25	rev. 473
"			MIDUSS crea	ted			S	unday	. Februar	v 07. 2010
"		10	Unite used.				5	anaay	, rebruur	io METRIC
		10	Job foldor:				0.1378	88/301	A SWM Doc	
			Output file	namo.			2. (370	378	98-300 De	+25mm2 011+
			Liconcoo na	mo.				5700	JO-JOU F2	Admin
			Company							Migrogoft
			Doto C Time	loct no	od.			10/0	/2014 at	2.EO.42 DM
	2.1	т.т.	ME DADAMETER	e last us	ea:			12/2,	/2014 al	5:50:45 PM
	51	E 000	ME PARAMEIER	5						
		5.000	Man Step"	1						
		240.000	Max. Storm	Iength"						
	2.0	1500.000	Max. Hydrog	frapn"						
	32	SI	ORM Chicago	storm"						
		L	Chicago sto	orm"						
		510.410	Coefficient	A"						
		5.500	Constant B"							
		0.800	Exponent C"							
		0.400	Fraction R"							
		240.000	Duration"							
		1.000	Time step m	ultiplie	r"		_	<i>i</i>		
		Ma	ximum intens	sity		74.66	0 mm	/hr"		
"		To	otal depth			25.00	0 mm	"		
"		5	25hyd Hyd	lrograph	extensi	on us	ed in t	his f	ile"	
"	33	CA	TCHMENT 201"							
"		1	Triangular	SCS"						
"		2	Proportiona	al to %"						
"		1	SCS method"							
"		201	BRIARHILL S	SUBDIVISI	on"					
"		55.000	% Imperviou	ıs"						
"		12.540	Total Area"							
"		36.000	Flow length	1 <b>"</b>						
"		2.000	Overland Sl	ope <b>"</b>						
"		5.643	Pervious Ar	rea"						
"		36.000	Pervious le	ength"						
"		2.000	Pervious sl	.ope"						
"		6.897	Impervious	Area"						
"		44.000	Impervious	length"						
"		2.000	Impervious	slope"						
"		0.250	Pervious Ma	nning 'n						
"		84.000	Pervious SC	CS Curve	No."					
"		0.237	Pervious Ru	noff coe	fficier	nt"				
"		0.100	Pervious Ia	ı∕S coeff	icient"					
"		4.838	Pervious In	itial ab	stracti	on"				
"		0.015	Impervious	Manning	'n'"					
"		98.000	Impervious	SCS Curv	e No."					
		0.795	Impervious	Runoff c	oeffici	.ent"				
		0.100	Impervious	Ia/S coe	fficier	it"				
		0.518	Impervious	Initial	abstrac	ction"			/ <u></u>	
			0.949	0.00	0 (	0.000	0.0	00 C.I	n/sec"	
		Ca	tchment 201		Pervic	ous	Impervi	ous To	otal Area	1 " 
		Su	irface Area		5.643		6.897	12	2.540	hectare"
		Ti	me of concer	itration	27.328	3	3.283	8	.000	minutes"
		Ti	me to Centro	oid	171.36	57	122.279	1.	31.909	minutes"
		Ra	infall depth	1	25.000	)	25.000	2	5.000	mm"
		Ra	infall volum	le	1410.7	/4	1724.24	3.	134.99	c.m"
		Ra	infall losse	es	19.072	2	5.127	1.	1.402	mm"
"		Ru	noff depth		5.928		19.872	1:	3.598	mm "
"		Ru	noff volume		334.53	3	1370.60	1	/05.13	c.m"
"		Ru	noff coeffic	cient	0.237		0.795	0	.544	"
"		Ма	ximum flow		0.075		0.941	0	.949	c.m/sec"
"	40	HY	DROGRAPH Add	l Runoff	"					
"		4	Add Runoff	п		_				
			0.949	0.94	9 C	0.000	0.0	00"		
	51	PI	PE DESIGN"							
"		0.949	Current pea	ık flow	c.m/s	sec"				
		0.013	Manning 'n'							
		1.200	Diameter	metre"						
		0.300	Gradient	~"						

"		De	epth of flow		0.50	50 metre"	I	
"		Ve	elocity		1.83	32 m/sec"	1	
		P	lpe capacity		2.13	35 c.m/se	*C <b>"</b>	
	F 2	Ci	ritical depth		0.52	27 metre"		
	53	CO OO	DUIE Pipe Ro	oute 60"	ah longth	(motro) "		
		0 000	Y-factor <- (	9 00 Kea 1 5 <b>"</b>	ich rengen	( metre)		
"		24.559	K-lag ( sec	conds)"				
"		0.000	Default(0) or	user s	spec.(1) val	lues used"		
"		0.500	X-factor <= (	).5"	-			
"		30.000	K-lag ( sec	conds)"				
"		0.662	Beta weightir	ng facto	or"	_		
		60.000	Routing time	step	( seconds)'	1		
		L	No. of sub-re	eaches"	0 00	a = m/ac	~ <b>"</b>	
"		Et	0 9/9	0 9/0	0.03			
"	40	H	DROGRAPH Com	ubine	1"	0.000 0		
"	10	6	Combine "		-			
"		1	Node #"					
"			SWM POND"					
"		Ma	aximum flow		0.89	98 c.m/se	C"	
"		ΗJ	/drograph volum	ne	1705.12	27 c.m"		
			0.949	0.949	0.898	0.898"		
	40	H	DROGRAPH Start	: – New Twibutar	Tributary"			
		Z	Start - New 1	n non	. Y	0 808"		
"	33	CZ	ATCHMENT 202"	0.000	0.000	0.000		
"		1	Triangular SC	CS"				
"		2	Proportional	to %"				
"		1	SCS method"					
"		202	Fair Grounds'	1				
		95.000	% Impervious'	1				
		7.130	Total Area"					
		60.000	Flow length" Overland Slor	NO."				
"		0.357	Pervious Area					
"		60.000	Pervious lend	rth"				
"		0.500	Pervious slop	be"				
"		6.773	Impervious Ar	ea"				
"		1140.000	Impervious le	ength"				
		0.500	Impervious sl	ope"				
		0.250	Pervious Manr	ning 'n'				
		84.000	Pervious SCS	Curve N	lo."			
"		0.237	Pervious Ta/9	COPTI COPT	cient"			
"		4.838	Pervious Init	ial abs	straction"			
"		0.015	Impervious Ma	nning '	n'"			
"		98.000	Impervious SC	CS Curve	e No."			
"		0.808	Impervious Ru	noff co	efficient"			
		0.100	Impervious Ia	a/S coef	ficient"			
		0.518	Impervious Ir	ntial a	bstraction'	0 000 -		
"		C	tchment 202	0.000	Pervious	Tmpervious	Total Area	
"		Si	irface Area		0.357	6.773	7.130	hectare"
"		T	lme of concentr	ation	56.278	35.068	35.390	minutes"
"		T	lme to Centroid	1	212.956	173.038	173.645	minutes"
"		Ra	ainfall depth		25.000	25.000	25.000	mm"
"		Ra	ainfall volume		89.12	1693.37	1782.49	c.m"
"		Ra	ainfall losses		19.071	4.809	5.522	mm"
"		Ru	noit depth		5.929	20.191	1200 75	mm"
		Ri , a	mort volume	n+	∠⊥.⊥4 0 237	130/.01 0 808	1300./5 0 779	C.M" "
"		KI Ma	anorr coerricie aximum flow	5116	0.003	0.314	0.316	C.m/sec"
"	40	H	DROGRAPH Add F	Runoff "				,
"	-	4	Add Runoff "					
"			0.316	0.316	0.898	0.898"		
"	52	CH	HANNEL DESIGN"					
		0.316	Current peak	flow	c.m/sec"			
		0.040	Manning 'n'"					

"		Ο.	Cross-section type:	0=trapezoid	lal; 1=gener	al"	
"		3.000	Basewidth metre"				
"		3.000	Left bank slope"				
"		3.000	Right bank slope"				
		0.750	Channel depth me	tre"			
		0.500	Gradient %"	0 1 5	70		
		De	epth of flow	0.17	a metre		
			erocity	0.50	14 m/sec		
"		CI	ritical depth	4.43	)1 metre	·	
"	53	R	OUTE Channel Route	250"	1 10010		
"		250.00	Channel Route 25	0 Reach lenc	th (metr	ce)"	
"		0.418	X-factor <= 0.5"	-			
"		186.091	K-lag (seconds)"				
"		0.000	Default(0) or user	spec.(1) val	ues used"		
"		0.500	X-factor <= 0.5"				
"		30.000	K-lag ( seconds)"				
"		0.500	Beta weighting fact	or"			
"		300.000	Routing time step	( seconds)"	1		
		2	No. of sub-reaches"	0.01	- /		
		Pe	eak outilow	0.31	.5 C.m/Se	ec"	
	10	LIN	U.SIO U.SI	1"	0.090 (	sec.	
"	40	п.	Combine "	T			
"		1	Node #"				
"		±	SWM POND"				
"		Ma	aximum flow	0.92	26 c.m/se	ec"	
"		H	ydrograph volume	3093.87	78 c.m"		
"		-	0.316 0.31	6 0.315	0.926"		
"	40	H	YDROGRAPH Start - New	Tributary"			
"		2	Start – New Tributa	ry"			
	~ ~		0.316 0.00	0 0.315	0.926"		
	33	CA	ATCHMENT 203"				
		1	Triangular SCS"				
		∠ 1	SCS mothod"				
"		203	Future Development"				
"		55,000	% Impervious"				
"		11.890	Total Area"				
"		610.000	Flow length"				
"		0.500	Overland Slope"				
"		5.351	Pervious Area"				
"		610.000	Pervious length"				
"		0.500	Pervious slope"				
		6.540	Impervious Area"				
		/45.556	Impervious length"				
"		0.300	Pervious Manning 'n				
"		84 000	Pervious SCS Curve 1	No "			
"		0.237	Pervious Runoff coe	fficient"			
"		0.100	Pervious Ia/S coeff	icient"			
"		4.838	Pervious Initial ab	straction"			
"		0.015	Impervious Manning	'n'"			
"		98.000	Impervious SCS Curv	e No."			
"		0.808	Impervious Runoff c	oefficient"			
"		0.100	Impervious Ia/S coe	fficient"			
		0.518	Impervious Initial	apstraction"	0 000	~ ~ / ~ ~ ~ "	
		0	0.3/3 0.00	v U.JLD	U.YZ6 (	Total Nroa	"
"		Ca C1	irface Area	5 351	6 540	11 890	hectare"
"		т-	ime of concentration	226,281	27.180	65.729	minutes"
"		T	ime to Centroid	456.264	160.404	217.687	minutes"
"		Ra	ainfall depth	25.000	25.000	25.000	mm"
"		Ra	ainfall volume	1337.62	1634.87	2972.49	c.m"
"		Ra	ainfall losses	19.073	4.802	11.224	mm "
"		Rı	unoff depth	5.927	20.198	13.776	mm"
		Rı -	unoti volume	317.13	1320.83	163/.96	c.m"
		Ri	unoii coeiiicient	0.23/	U.8U8	0.351	 
		1416	AATHUHH TIOW	U.UIZ	0.3/3	0.3/3	C.III/SeC"

"	40	HJ	DROGRAPH Ad	d Runoff	"		
		4	Add Runoff			0.015	
	F 0	<u></u>	0.3/5	0.3	/5	0.315	0.926"
	52	0 275	ANNEL DESIG	N"	~ ~~	/	
		0.375	Manning In	ak IIOw	С.Ш	/sec	
"		0.015	Cross-sect	ion type	• 0-tr	anezoidal.	1-general"
"		2 000	Basewidth	metre	. 0-tr "	apezoidai,	I-general
"		50 000	Left bank	slope"			
"		50.000	Right bank	slope"			
"		0.300	Channel de	oth me	etre"		
"		0.500	Gradient	8 <b>"</b>			
"		De	pth of flow	r		0.088	metre"
"		Ve	locity			0.660	m/sec"
"		Cł	annel capac	ity		7.066	c.m/sec"
"		Cr	itical dept	h		0.085	metre"
"	53	RC	OUTE Chan	nel Route	e 50"		
"		50.00	Channel	Route 50	0 Reac	h length	( metre)"
		0.422	X-factor <	= 0.5"	-		
		56.823	K-lag (	seconds)			
		0.000	Default(0)	or user	spec.	(1) values	used"
		0.500	X-Iactor <	= 0.5"			
		50.000	R-Lay (	ting fact	tor"		
"		60.000	Bouting ti	me sten	lui ( se	conds)"	
"		1	No of sub	-reaches	"	condby	
"		Pe	ak outflow	reacheb		0.371	c.m/sec"
"			0.375	0.3	75	0.371	0.926 c.m/sec"
"	40	HY	DROGRAPH	Combine	1"		
"		6	Combine "				
"		1	Node #"				
"			SWM POND"				
"		Ma	ximum flow	_		1.067	c.m/sec"
		ΗΣ	drograph vo	lume		4731.842	c.m"
	4.0			0.3	/5	0.3/L	1.06/"
	40	н 1 7	Confluonco	continend	ce	Τ	
"		, 1	Node #"				
"		T	SWM POND"				
"		Ma	ximum flow			1.067	c.m/sec"
"		Hv	drograph vo	lume		4731.842	c.m"
"		4	0.375	1.00	67	0.371	0.000"
"	54	PC	ND DESIGN"				
"		1.067	Current pe	ak flow	c.m	/sec"	
"		2.000	Target out	flow o	c.m/se	с"	
"		4731.8	Hydrograph	volume	c.m	II	
		16.	Number of	stages"			
		100.000	Minimum wa	ter leve.	L m	etre"	
		100.000	Maximum wa	ler leve.		etre" motro <b>"</b>	
"		100.000	Keen Desig	n Data•	=⊥ 1 = Tr	$11e \cdot 0 = Fa$	190"
"		0	Level Di	scharge	Vol	uc, o - ra ume"	196
"			100.000	0.000	0.	000"	
"			100.200	0.02045	1074.	207"	
"			100.400	0.06830	2187.	288"	
"			100.600	0.1209	3339.	734"	
"			100.800	0.1986	4532.	208"	
"			101.000	0.3288	5765.	196"	
"			101.200	0.5024	7039.	318"	
"			101.400	0.7069	8355.	202"	
			101.600	0.9282	9/13.	323"	
			102.000	1,151	10550	.30" 70 <b>"</b>	
			102.000	1.303 1 EE0	14047	• /ð" 22 <b>1</b>	
			102.200	⊥.000 1 735	15520	· ∠ ∠ 31 "	
"			102 600	1 896	17158	.50"	
"			102.800	2.045	18782	.50"	
"			103.000	2.183	20452	.76"	
"		1.	LAYERS"	0 0		-	

"	Bottom	Aspect	Bottom	Тор	Average"	
"	area	ratio	elevation	elevation	sideslope"	
"	2. OUTFLOW	PIPE"	100.000	103.000	5.000	
"	Upstream	Downstr'm	Pipe	Pipe	Manning	Entry"
	invert 100_000	invert 99 700	Length	Diameter	'n' 0 013	loss Ke" 0 500"
"	100.600	100.300	30.000	0.900	0.013	0.500"
"	Peak outfl	OW	0	.118 c	.m/sec"	
"	Maximum le	vel	100	.590 m	etre"	
"	Centroidal	laq	12	.400 c	urs"	
"	0.375	1.067	0.118	0.000	c.m/sec"	
"	40 HYDROGRAPH	Next link	n			
"	J NEXU II	375 0.1	.18 0.1	18 0.	000"	
"	33 CATCHMENT	204"				
"	1 Triangu	lar SCS"				
"	1 SCS met	hod"				
"	204 Future	Development				
"	55.000 % Imper	vious"				
"	36.000 Flow le	rea" nath <b>"</b>				
"	2.000 Overlan	d Slope"				
"	0.356 Perviou	s Area"				
"	2.000 Perviou	s slope"				
"	0.435 Impervi	ous Area"				
"	44.000 Impervi	ous length"	1			
"	0.250 Perviou	s Manning '	n'"			
"	84.000 Perviou	s SCS Curve	e No."			
"	0.237 Perviou	s Runoff co	efficient"			
"	4.838 Perviou	s Initial a	abstraction	"		
"	0.015 Impervi	ous Manning	g 'n'"			
"	98.000 Impervi	ous SCS Cur	ve No."	+ "		
"	0.100 Impervi	ous Ia/S co	efficient"	L		
"	0.518 Impervi	ous Initial	abstracti	on"		
	U. Catchment	060 0.1 204	.18 0.1 Pervious	18 0. Imperv	000 c.m/sec"	iros "
"	Surface Ar	ea	0.356	0.435	0.790	hectare"
"	Time of co	ncentration	n 27.328	3.283	8.000	minutes"
"	Time to Ce	ntroid opth	171.367	122.27	9 131.909	minutes"
"	Rainfall v	olume	88.87	108.62	197.50	c.m"
"	Rainfall 1	osses	19.072	5.127	11.402	mm "
	Runoff dep Runoff vol	th	5.928	19.872	13.598 107 42	mm"
"	Runoff coe	fficient	0.237	0.795	0.544	"
"	Maximum fl	ow	0.005	0.059	0.060	c.m/sec"
	40 HYDROGRAPH 4 Add Bun	Add Runoff off "	"			
"	0.	060 0.1	.21 0.1	18 0.	000"	
"	52 CHANNEL DE	SIGN"	,			
	0.121 Current 0.015 Manning	peak ilow 'n'"	c.m/sec			
"	0. Cross-s	ection type	e: 0=trapez	oidal; 1=	general"	
"	8.000 Basewid	th metre	<u>،</u> ۳			
"	50.000 Leit ba 50.000 Right b	nk slope" ank slope"				
"	0.300 Channel	depth m	netre"			
"	0.500 Gradien	t %"	-	000		
"	Depth of f Velocity	MOT	0	.030 m	etre" /sec <b>"</b>	
"	Channel ca	pacity	10	.429 c	.m/sec"	
"	Critical d	epth	0	.027 m	etre"	

```
" 53
            ROUTE
                          Channel Route 170"
         170.00 Channel Route 170 Reach length (metre)"
...
          0.490 X-factor <= 0.5"
...
         305.982 K-lag (seconds)"
"
          0.000 Default(0) or user spec.(1) values used"
          0.500 X-factor <= 0.5"
30.000 K-lag (second
"
...
                     K-lag (seconds)"
          0.500 Beta weighting factor"
...
        300.000 Routing time step ( seconds)"
1 No. of sub-reaches"
...
...
                                        0.121 c.m/sec"
0.121 0.121 0.000 c.m/sec"
"
                 Peak outflow
...
                            0.060
                HYDROGRAPH Combine 2"
6 Combine "
 40
...
...
                2 Node #"
"
                                                                  c.m/sec"
"
                 Maximum flow
                                                        0.121
                 Hydrograph volume
                                                  4197.022
0.121
...
                                                                    c.m"
...
                          0.060 0.121
                                                                   0.121"
" 40
                 HYDROGRAPH Start - New Tributary"
"
                2 Start - New Tributary"
"
                                      0.000
                                                     0.121 0.121"
                          0.060
" 33
                 CATCHMENT 205"
                1 Triangular SCS"
...
                2 Proportional to %"
...
                1
                   SCS method"
...
              205 Fair Grounds - Uncontrolled"
          0.000 % Impervious"
0.680 Total Area"
"
...
         10.000 Flow length"
"
...
          0.500 Overland Slope"
...
          0.680 Pervious Area"
"
         10.000 Pervious length"
...
          0.500 Pervious slope"
...
                     Impervious Area"
          0.000
"
          0.000 Impervious length"
"
          0.500 Impervious slope"
...
          0.250 Pervious Manning 'n'"
          84.000 Pervious SCS Curve No."
0.237 Pervious Runoff coeffic
...
"
                     Pervious Runoff coefficient"
          0.100 Pervious Ia/S coefficient"
"
...
          4.838 Pervious Initial abstraction"
"
          0.015 Impervious Manning 'n'"
"
          98.000 Impervious SCS Curve No."
"
          0.000 Impervious Runoff coefficient"
0.100 Impervious Ia/S coefficient"
...
          0.518 Impervious Initial abstraction"
...
...
                          0.011 0.000 0.121
                                                                 0.121 c.m/sec"

      Catchment 205
      Pervious
      Impervious Total Area

      Surface Area
      0.680
      0.000
      0.680
      hectare"

      Time of concentration
      19.207
      0.001
      19.207
      minutes"

      Time to Centroid
      159.747
      116.341
      159.747
      minutes"

      Rainfall depth
      25.000
      25.000
      mm"

      Rainfall volume
      170.00
      0.001
      170.00
      c.m"

...
"
...
...
...
"
                                              19.0816.8205.91918.18040.250.00
"
                                                                            19.081
                 Rainfall losses
                                                                                         mm"
                 Runoff depth
Runoff volume
                                                                            5.919
40.25
...
                                                                                          mm"
                                                                                          c.m'
...
                                                           0.000
                                                                                         "
                 Runoff coefficient
                                              0.237
                                                                           0.237
...
                                                                          0.011 c.m/sec"
                 Maximum flow
                                               0.011
                                                           0.000
" 40
                HYDROGRAPH Add Runoff "
"
                4 Add Runoff "
...
                                         0.011 0.121
                            0.011
                                                                 0.121"
                CHANNEL DESIGN"
...
 52
...
           0.011 Current peak flow c.m/sec"
...
           0.040 Manning 'n'"
              0. Cross-section type: 0=trapezoidal; 1=general"
"
          0.000 Basewidth met
50.000 Left bank slope"
"
                     Basewidth metre"
...
          50.000 Right bank slope"
```

"	0.300	Channel depth	metre"			
"	0.500	Gradient %"				
"	De	epth of flow		0.041	metre"	
"	Ve	locity		0.132	m/sec"	
"	Ch	annel capacity		2.245	c.m/sec"	
"	Cr	itical depth		0.025	metre"	
"	53 RC	OUTE Channel Rou	te 360"			
"	360.00	Channel Route	360 Reach	length	( metre)"	
"	0.470	X-factor <= 0.5"		-		
"	292.179	K-lag (seconds	:) "			
"	0.000	Default(0) or use	r spec.(1)	values u	ised"	
"	0.500	X-factor <= 0.5"				
"	30.000	K-lag (seconds	:) "			
"	0.500	Beta weighting fa	ctor"			
"	300.000	Routing time step	) (secon	ıds)"		
"	7	No. of sub-reache	s"			
"	Pe	eak outflow		0.011	c.m/sec"	
"		0.011 0.	011 0.	011 (	0.121 c.m/sec	II
"	40 HY	DROGRAPH Combine	2"			
"	6	Combine "				
"	2	Node #"				
"		"				
"	Ma	aximum flow		0.122	c.m/sec"	
"	Ну	drograph volume	423	57.274	c.m"	
"		0.011 0.	011 0.	011 (	0.122"	
"	38 SI	ART/RE-START TOTAL	S 205"			
"	3	Runoff Totals on	EXIT"			
"	Tc	otal Catchment area			33.030	hectare"
"	Tc	tal Impervious are	a		20.644	hectare"
"	Tc	tal % impervious			62.502"	
"	19 EX	XIT"				

"			MIDUISS Output				>"
"			MIDUSS version			Version 2.25	rev. 473"
"			MIDUSS created		S	undav. February	v 07. 2010"
"		10	Units used:		-		ie METRIC"
"			Job folder:		0:\378	88\300\SWM Des:	ign\MIDUSS"
"			Output filename:		~	37888-300 Pst	250Yr7.out"
"			Licensee name:				Admin"
"			Company				Microsoft"
"			Date & Time last use	ed:		12/2/2014 at 3	3:44:56 PM"
"	31	TI	ME PARAMETERS"			, _, _ 0 0 0 0	
"		5.000	Time Step"				
"		1440.000	Max. Storm length"				
"		1500.000	Max. Hydrograph"				
"	32	ST	ORM Chicago storm"				
"	01	1	Chicago storm"				
"		2095.179	Coefficient A"				
"		13.509	Constant B"				
"		0.773	Exponent C"				
"		0.400	Fraction R"				
"		1440.000	Duration"				
"		1.000	Time step multiplie	r "			
"		Ma	ximum intensity	213	.438 mm	/hr"	
"		То	tal depth	180	.669 mm	, 11	
"		6	250hvd Hvdrograph	extension	n used in '	this file"	
"	33	CA	TCHMENT 201"				
"		1	Triangular SCS"				
"		2	Proportional to %"				
"		1	SCS method"				
"		201	BRIARHILL SUBDIVISIO	ON"			
"		55.000	% Impervious"				
"		12.540	Total Area"				
"		36.000	Flow length"				
"		2.000	Overland Slope"				
"		5.643	Pervious Area"				
"		36.000	Pervious length"				
"		2.000	Pervious slope"				
"		6.897	Impervious Area"				
"		44.000	Impervious length"				
"		2.000	Impervious slope"				
		0.250	Pervious Manning 'n				
		84.000	Pervious SCS Curve I	No."			
		0.760	Pervious Runoff coel	fficient"			
		0.100	Pervious la/S coeff:	icient"			
		4.838	Pervious Initial abs	straction	•		
		0.015	Impervious Manning	n'''			
		98.000	Impervious SCS Curve	E NO."			
		0.957	Impervious Ruholi Co	Sellicient"			
		0.100	Impervious Ia/S coel	LIICIent"	II		
		0.510				00 a m/aca"	
"		Ca	4.975 0.000	Porvious	Importi	ous Total Aroa	"
"		Ca Su:	rface Area	5 6/3	6 897	12 5/0	hectare"
"		5u. Ti	mo of concontration	10 607	2 065	5 /29	minutos"
"		11) Ti	me to Controid	716 219	2.000	679 183	minutes
"		I II Ra	infall denth	180 669	180 669	180 669	mm"
"		Ra	infall volume	1 0195	1 2461	2 2656	ha_m"
"		Ra	infall losses	43 332	7 715	23 742	mm"
"		Rui	noff depth	137.337	172.954	156.927	 mm <b>"</b>
"		R11	noff volume	0.7750	1,1929	1,9679	ha-m"
"		R11	noff coefficient	0.760	0.957	0.869	"
"		Ma	ximum flow	2.095	3.624	4,973	c.m/sec"
"	40	HY	DROGRAPH Add Runoff '	"			, 000
"	-	4	Add Runoff "				
"			4.973 4.973	3 0.00	0.0	00"	
"	56	DI	VERSION"				
"		201	Node number"				
"		2.114	Overflow threshold"				
"		1.000	Required diverted fi	raction"			
"		1	Conduit type; 1=Pipe	e;2=Channe	el"		

2.135 Conduit capacity"
1.200 Conduit height/diameter" " ... 0.300 Conduit Grade (%)" ... ... Peak of diverted flow 2.859 c.m/sec" " Volume of diverted flow 2628.377 c.m" " DIV00201.250hyd" ... Major flow at 201" 4.973 4.973 ... 2.114 0.000 c.m/sec" **"** 40 HYDROGRAPH Next link " ... 5 Next link " " 4.973 2.114 2.114 0.000" " 51 PIPE DESIGN" 2.114 Current peak flow c.m/sec" ... 0.013 Manning 'n'" ... 1.200 Diameter metre" " 0.300 Gradient %" ... metre" Depth of flow 0.973 m/sec" ... Velocity 2.153 " Pipe capacity 2.135 c.m/sec" ... Critical depth 0.801 metre" **"** 53 ROUTE Pipe Route 60" 60.00 Pipe Route 60 Reach length ( metre)" ... 0.000 X-factor <= 0.5" 20.906 K-lag (seconds)" ... ... 0.000 Default(0) or user spec.(1) values used" ... ... 0.500 X-factor <= 0.5" ... 30.000 K-lag ( seconds)" 0.919 Beta weighting factor" 100.000 Routing time step (seconds)" 1 No. of sub-reaches" " ... ... Peak outflow 2.114 0.000 c.m/sec" ... ... **"** 40 HYDROGRAPH Combine 1" 6 Combine " 1 Node #" ... 1 Node #" " SWM POND" ... Maximum flowZ.114C.1078Hydrograph volume17050.020c.m"2.1142.1142.114 Maximum flow 2.114 c.m/sec" ... ... 4.973 2.114 2.114 2.114" HYDROGRAPH Start - New Tributary" " 40 2 Start - New Tributary" " ... 4.973 0.000 2.114 2.114" " 33 CATCHMENT 202" ... 1 Triangular SCS" ... Proportional to %" 2 ... 1 SCS method" 202 Fair Grounds" ... ... 95.000 % Impervious" ... 7.130 Total Area" 60.000 Flow length" 0.500 Overland Slope" 0.357 Pervious Area" " ... ... ... 60.000 Pervious length" " 0.500 Pervious slope" 6.773 Impervious Area" 1140.000 Impervious length" 0.500 Impervious slope" " ... ... ... 0.250 Pervious Manning 'n'" ... 84.000 Pervious SCS Curve No." " 0.755 Pervious Runoff coefficient" " 0.100 Pervious Ia/S coefficient" 4.838 Pervious Initial abstracti " Pervious Initial abstraction" " 0.015 Impervious Manning 'n'" ... 98.000 Impervious SCS Curve No." " 0.960 Impervious Runoff coefficient" " 0.100 Impervious Ia/S coefficient" ... Impervious Initial abstraction" 0.518 2.454 0.000 2.114 2.114 c.m/sec" Pervious Impervious Total Area " Catchment 202

	40	Surface Area Time of concentration Time to Centroid Rainfall depth Rainfall volume Rainfall losses Runoff depth Runoff volume Runoff coefficient Maximum flow HYDROGRAPH Add Runoff 4 Add Runoff "	0.357 21.844 733.888 180.669 0.0644 44.192 136.477 0.0487 0.755 0.101	6.773 22.056 692.757 180.669 1.2238 7.254 173.415 1.1746 0.960 2.353	7.130 22.047 694.392 180.669 1.2882 9.101 171.568 1.2233 0.950 2.454	hectare" minutes" mm" ha-m" mm" ha-m" " c.m/sec"
"		2.454 2.4	54 2.114	2.114"	ı	
"	52	CHANNEL DESIGN"	a m/aca"			
"		0.040 Manning 'n'"	C.III/Sec			
"		0. Cross-section type	: 0=trapezoi	dal; 1=gene	eral"	
		3.000 Basewidth metre 3.000 Left bank slope"				
"		3.000 Right bank slope"				
"		0.750 Channel depth m	etre"			
"		Depth of flow	0.5	52 metre	è	
"		Velocity	0.9	54 m/sec	2"	
"		Critical depth	4.4	60 metre	ec" ,"	
"	53	ROUTE Channel Rout	e 250"			
		250.00 Channel Route 2 0.384 X-factor <= 0.5"	50 Reach len	.gth (met	re)"	
"		196.612 K-lag (seconds)	"			
"		0.000 Default(0) or user 0.500 X-factor <= 0.5"	spec.(1) va	lues used"		
"		30.000 K-lag (seconds)	"			
"		0.500 Beta weighting fac	tor" (seconds)	"		
"		1 No. of sub-reaches	"			
"		Peak outflow	2.3	89 c.m/s	sec"	
"	40	HYDROGRAPH Combine	1" 2.309	2.114	C.III/Sec	
"		6 Combine "				
"		SWM POND"				
"		Maximum flow	4.4	08 c.m/s	sec"	
"		Hydrograph volume 2.454 2.4	29276.9 54 2.389	63 C.m" 4.408'	,	
"	40	HYDROGRAPH Start - Ne	w Tributary"			
"		2 Start - New Tribut 2.454 0.0	ary" 00 2.389	4.408"		
"	33	CATCHMENT 203"				
"		I Triangular SCS" 2 Proportional to %"				
"		1 SCS method"	_			
"		203 Future Development	"			
"		11.890 Total Area"				
"		610.000 Flow length"				
"		5.351 Pervious Area"				
"		610.000 Pervious length"				
"		6.540 Impervious Area"				
"		745.556 Impervious length"				
"		0.250 Impervious slope" 0.250 Pervious Manning "	n'"			
"		84.000 Pervious SCS Curve	No."			
"		0.707 Pervious Runoff co 0.100 Pervious Ta/S coef	efficient" ficient"			
"		4.838 Pervious Initial a	bstraction"			
"		0.015 Impervious Manning	'n'"			
			•			

98.000 Impervious SCS Curve No." 0.963 Impervious Runoff coefficient" " ... 0.100 Impervious Ia/S coefficient" ... ... 0.518 Impervious Initial abstraction" " 2.670 0.000 2.389 4.408 c.m/sec" Pervious Impervious Total Area " 5.351 6.540 11.890 hectare" tration 87.829 17.095 43.634 minutes" " Catchment 203 ... Surface Area ... Time of concentration 87.829 Time to Centroid 820.991 684.664 735.814 minutes" Rainfall depth180.669180.669180.669minutRainfall volume0.96671.18152.1482ha-m"Rainfall losses52.9246.62327.459mm"Runoff depth127.745174.046153.210mm"Runoff coefficient0.7070.9630.848"Maximum flow0.5062.5550.555 ... ... " ... ... ... ... Maximum flow 2.555 2.670 c.m/sec" 0.506 **"** 40 HYDROGRAPH Add Runoff " 4 Add Runoff " 2.670 ... 2.670 2.389 ... 4.408" **"** 52 CHANNEL DESIGN" ... 2.670 Current peak flow c.m/sec" ... 0.015 Manning 'n'" Cross-section type: 0=trapezoidal; 1=general"
 2.000 Basewidth metre" ... ... 50.000 Left bank slope" ... ... 50.000 Right bank slope" ... 0.300 Channel depth metre" " 0.500 Gradient %" ... Depth of flow 0.203 metre" 1.085 m/sec" ... Velocity Channel capacity ... 7.066 c.m/sec" ... Critical depth 0.206 metre" " 53 ROUTE Channel Route 50" 50.00 Channel Route 50 Reach length (metre)" 0.335 X-factor <= 0.5" ... ... 34.557 K-lag (seconds)" " ... 0.000 Default(0) or user spec.(1) values used" ... 0.500 X-factor <= 0.5" 30.000 K-lag (seconds)" 0.500 Beta weighting factor" 42.857 Routing time step (seconds)" 1 No. of sub-reaches" ... " " ... 
 Peak outflow
 2.607
 c.m/sec"

 2.670
 2.670
 2.607
 4.408
 c.m/sec"
 ... " **"** 40 HYDROGRAPH Combine 1" 6 Combine " Node #" ... 1 ... SWM POND" ... Maximum flow Maximum flow 6.991 c.m/ Hydrograph volume 47491.840 c.m" 6.991 c.m/sec" ... 4/491.840 2.670 2.670 2.607 HYDROGRAPH Confluence 1" 7 Confluence " ... 6.991" **"** 40 ... 7 Confluence " " 1 Node #" " SWM POND" c.m/sec" ... Maximum flow6.991Hydrograph volume47491.836 c.m" ... 2.670 6.991 2.607 0.000" **"** 54 POND DESIGN" " 6.991 Current peak flow c.m/sec" 2.000 Target outflow c.m/sec" 47491.8 Hydrograph volume c.m" 16. Number of stages" " ... " ... 100.000 Minimum water level metre" " 103.000 Maximum water level metre" " 100.000 Starting water level metre" ... Keep Design Data: 1 = True; 0 = False" 0 Level Discharge Volume" 100.000 0.000 0.000"

"	100.200 0.02045	1074.207"			
"	100.400 0.06830	2187.288"			
	100.600 0.1209	3339.734"			
	100.800 0.1986	4532.208"			
	101.000 0.3288	5/65.196" 7020 210 <b>0</b>			
	101.200 0.3024	2355 202 <b>"</b>			
	101 600 0 9282	9713 323 <b>"</b>			
"	101.800 1.151	11114.36"			
"	102.000 1.363	12558.78"			
"	102.200 1.558	14047.22"			
"	102.400 1.735	15580.31"			
"	102.600 1.896	17158.50"			
"	102.800 2.045	18782.50"			
	103.000 2.183	20452.76"			
	I. LAYERS" Bottom Accort	Pottom	Top	araga"	
	area ratio	elevation el	evation side	veraye slope"	
"	5275.000 2.400	100.000	103.000	3.000"	
"	2. OUTFLOW PIPE"	100.000	100.000	3.000	
"	Upstream Downstr'm	Pipe	Pipe Ma	anning	Entry"
"	invert invert	Length D	iameter	'n ĺlo	ss Kē"
"	100.000 99.700	30.000	0.375	0.013	0.500"
"	100.600 100.300	30.000	0.900	0.013	0.500"
"	Peak outflow	1.9	088 c.m/se	ec"	
	Maximum level	102.7	24 metre	n	
	Maximum storage	18164.6	045 C.M"		
	2 670 6 991	1 988		/	
"	40 HYDROGRAPH Next link	"	0.000 C.III,	360	
"	5 Next link "				
"	2.670 1.	988 1.988	0.000"		
"	33 CATCHMENT 204"				
"	1 Triangular SCS"				
	2 Proportional to %				
	I SCS method"	+ "			
	55 000 & Impervious"				
"	0.790 Total Area"				
"	36.000 Flow length"				
"	2.000 Overland Slope"				
"	0.356 Pervious Area"				
"	36.000 Pervious length"				
	2.000 Pervious slope"				
	0.435 Impervious Area"				
	44.000 Impervious length				
"	0 250 Pervious Manning	'n'"			
"	84.000 Pervious SCS Curv	e No."			
"	0.760 Pervious Runoff c	oefficient"			
"	0.100 Pervious Ia/S coe	fficient"			
"	4.838 Pervious Initial	abstraction"			
	0.015 Impervious Mannin	.g 'n'"			
	98.000 Impervious SCS Cu	rve No."			
	0.957 Impervious Runoii	coefficient"			
	0.100 Impervious Ia/S C 0.518 Impervious Initia	l abstraction	, m		
"	0.313 1.	988 1.988	0.000	a.m/sec"	
"	Catchment 204	Pervious	Impervious	Total Area	п
"	Surface Area	0.356	0.435	0.790	hectare"
"	Time of concentratio	n 10.607	2.065	5.429	minutes"
"	Time to Centroid	716.219	655.123	679.184	minutes"
"	Rainfall depth	180.669	180.669	180.669	mm" _
"	Rainfall volume	642.28	/85.01	1427.28	C.M"
	Kalilali losses Pupoff dopth	43.33Z 137 337	/./10 172 05/	23./42 156 027	mm "
"	Runoff volume	488 23	1/2·234 751.49	1239.72	 
"	Runoff coefficient	0.760	0.957	0.869	"
"	Maximum flow	0.132	0.228	0.313	c.m/sec"

**"** 40 HYDROGRAPH Add Runoff " 4 Add Runoff " ... 0.313 2.028 1.988 0.000" **"** 52 CHANNEL DESIGN" " 2.028 Current peak flow c.m/sec" ... 0.015 Manning 'n'" ... Ο. Cross-section type: 0=trapezoidal; 1=general" 8.000 Basewidth metre" " ... 50.000 Left bank slope" " 50.000 Right bank slope" " 0.300 Channel depth metre" 0.500 Gradient %" ... Depth of flow 0.139 metre" 0.979 m/sec" ... Velocity ... Channel capacity Critical depth 10.429 c.m/sec" " 0.140 metre" **"** 53 ROUTE Channel Route 170" 170.00 Channel Route 170 Reach length ( metre)" ... 0.460 X-factor <= 0.5" 130.192 K-lag (seconds)" ... " 0.000 Default(0) or user spec.(1) values used" ... 0.500 X-factor <= 0.5" 30.000 K-lag ( seconds)" 0.500 Beta weighting factor" ... ... 100.000 Routing time step ( seconds)" 1 No. of sub-reaches" ... ... ... Peak outflow 2.027 c.m/sec" 2.028 " 2.027 0.000 c.m/sec" 0.313 HYDROGRAPH Combine 2" 6 Combine " **"** 40 ... 2 Node #" ... " 2.027 c.m/sec" Maximum flow Hydrograph volume caph volume44367.5040.3132.0282.027 ... c.m" 2.027" **"** 40 HYDROGRAPH Start - New Tributary" ... 2 Start - New Tributary" ... 0.313 0.000 2.027 2.027" " 33 CATCHMENT 205" 1 Triangular SCS"
2 Proportional to %" ... " ... 1 SCS method" " 205 Fair Grounds - Uncontrolled" 0.000 % Impervious" 0.680 Total Area" 10.000 Flow length" " ... ... 0.500 Overland Slope" ... ... 0.680 Pervious Area" ... 10.000 Pervious length" " 0.500 Pervious slope" 0.000 Impervious Area" 0.000 Impervious length" ... ... ... 0.500 Impervious slope" " 0.250 Pervious Manning 'n'" " 84.000 Pervious SCS Curve No." 0.761 Pervious Runoff coefficient" 0.100 Pervious Ia/S coefficient" ... ... 4.838 Pervious Initial abstraction" ... ... 0.015 Impervious Manning 'n'" " 98.000 Impervious SCS Curve No." " 0.000 Impervious Runoff coefficient" 0.100 Impervious Ia/S coefficient" ... Impervious Ia/S coefficient" ... 0.518 Impervious Initial abstraction" ... catchment 205PerviousImpervious Total AreaSurface Area0.6800.0000.660 0.301 0.000 2.027 2.027 c.m/sec" " 
 Surface Area
 0.680
 0.000
 0.680
 hectare"

 Time of concentration
 7.455
 0.000
 7.455
 minutes"

 Time to Centroid
 710.170
 649.556
 710.170
 minutes"

 Rainfall depth
 180.669
 180.669
 mm"
 " ...

"		Rainfall volur	ne :	1228.55	0.00	1228.55	c.m"
"		Rainfall losse	es é	43.234	23.093	43.234	mm"
"		Runoff depth		137.435	157.575	137.435	mm "
"		Runoff volume	(	934.56	0.00	934.56	c.m"
"		Runoff coeffic	cient (	0.761	0.000	0.761	"
"		Maximum flow	(	0.301	0.000	0.301	c.m/sec"
"	40	HYDROGRAPH Add	d Runoff "				
"		4 Add Runoff	"				
"		0.301	0.301	2.027	2.027"		
"	52	CHANNEL DESIGN	1"				
"		0.301 Current pea	ak flow	c.m/sec"			
"		0.040 Manning 'n'	T T				
"		0. Cross-sect	lon type: (	0=trapezoic	lal; 1=gener	cal"	
"		0.000 Basewidth	metre"	-	. 5		
"		50.000 Left bank s	slope"				
"		50.000 Right bank	slope"				
"		0.300 Channel der	oth meti	re"			
"		0.500 Gradient	8 <b>"</b>				
"		Depth of flow		0.14	ll metre'	•	
"		Velocity		0.30	)2 m/sec'	•	
"		Channel capac	lty	2.24	l5 c.m/se	ec"	
"		Critical depth	1	0.09	4 metre	•	
"	53	ROUTE Chanr	nel Route 3	360"			
"		360.00 Channel	Route 360	Reach leng	gth (meti	re)"	
"		0.456 X-factor <=	= 0.5"				
"		298.080 K-lag (s	seconds)"				
"		0.000 Default(0)	or user s	pec.(1) val	ues used"		
"		0.500 X-factor <=	= 0.5"				
"		30.000 K-lag (s	seconds)"				
"		0.500 Beta weight	ing facto	r"			
"		300.000 Routing tir	ne step	( seconds) '	1		
"		3 No. of sub-	-reaches"				
"		Peak outflow		0.28	30 c.m/se	ec"	
"		0.301	0.301	0.280	2.027 0	c.m/sec"	
"	40	HYDROGRAPH (	Combine	2"			
"		6 Combine "					
"		2 Node #"					
"		TI III					
"		Maximum flow		2.07	73 c.m/se	∋c"	
"		Hydrograph vol	lume	45301.49	06 c.m"		
"		0.301	0.301	0.280	2.073"		
"	38	START/RE-START	TOTALS 20	05"			
"		3 Runoff Tota	als on EXI	Γ"			
"		Total Catchmer	nt area		33	.030	hectare"
"		Total Impervio	ous area		20	.644	hectare"
"		Total % imperv	vious		62	.502"	
"	19	EXIT"					